

TRANSMITTAL LETTER TO THE UNITED STATES DESIGNATED / ELECTED OFFICE (DO/EO/US)- CONCERNING A FILING UNDER 35 U.S.C. 371		ATTORNEY'S DOCKET NUMBER P66886US0
		US APPLICATION NO (If known, see 37 CFR 1.51) 09/869317
INTERNATIONAL APPLICATION NO. PCT/EP00/11626	INTERNATIONAL FILING DATE 22 November 2000	PRIORITY DATE CLAIMED 25 November 1999
TITLE OF INVENTION METHOD FOR DETECTING FLUORESCENCE PHENOMENA IN MICROSCOPE		
APPLICANT(S) FOR DO/EO/US Volker GERSTNER and Ralf WOLLESCHENSKY		

Applicant herein submits to the United States Designated/Elected Office (DO/EO/US) the following items and other information.

1. ☒ This is a **FIRST** submission of items concerning a filing under 35 U.S.C. 371.
2. ☐ This is a **SECOND** or **SUBSEQUENT** submission of items concerning a filing under 35 U.S.C. 371.
3. ☒ This express request to begin national examination procedures (35 U.S.C. 371(f)) at any time rather than delay examination until the expiration of the applicable time limit set in 35 U.S.C. 371(b) and PCT Articles 22 and 39(1).
4. ☐ A proper Demand for Internatl. Preliminary Examination was made by the 19th month from earliest claimed priority date.
5. ☒ A copy of the International Application as filed (35 U.S.C. 371(c)(2))
 - a. ☒ is transmitted herewith (required only if not transmitted by the International Bureau).
 - b. ☒ has been transmitted by the International Bureau.
 - c. ☐ is not required, as the application was filed in the United States Receiving Office (RO/US)
6. ☐ A translation of the International Application into English (35 U.S.C. 371(c)(2)).
7. ☒ Amendments to the claims of the International Application under PCT Article 19 (35 U.S.C. 371(c)(3))
 - a. ☐ are transmitted herewith (required only if not transmitted by the International Bureau).
 - b. ☐ have been transmitted by the International Bureau.
 - c. ☐ have not been made; however, the time limit for making such amendments has NOT expired.
 - d. ☒ have not been made and will not be made.
8. ☐ A translation of the amendments to the claims under PCT Article 19 (35 U.S.C. 371(c)(3)).
9. ☐ An oath or declaration of the inventor(s) (35 U.S.C. 371(c)(4)).
10. ☐ A translation of the annexes to the Internatl. Preliminary Examination report under PCT Article 36 (35 U.S.C. 371(c)(5)).

Items 11. to 16. below concern other document(s) or information included:

11. ☐ An Information Disclosure Statement under 37 CFR 1.97 and 1.98.
12. ☐ An assignment document for recording. A separate cover sheet compliance with 37 CFR 3.28 and 3.31 is included.
13. ☐ A FIRST preliminary amendment.
☐ A SECOND or SUBSEQUENT preliminary amendment.
14. ☐ A substitute specification.
15. ☐ A change of power of attorney and/or address letter.
16. ☒ Other items or information:

International Search Report - EPO
PCT Request Form
First Page of Publication

US APPLICATION NO (If known, see 37 CFR 1.5) <div style="font-size: 2em; font-weight: bold; text-align: center;">09/869317</div>		INTERNATIONAL APPLICATION NO <div style="font-weight: bold; text-align: center;">PCT/EP00/11626</div>		ATTORNEY'S DOCKET NUMBER <div style="font-weight: bold; text-align: center;">P66886US0</div>	
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17. <input checked="" type="checkbox"/> The following fees are submitted: Basic National Fee (37 CFR 1.492(a)(1)-(5)): Internatl. prelim. examination fee paid to USPTO (37 CFR 1.492 (a) (1)) .. \$690.00 No international preliminary examination fee paid to USPTO (37 CFR 1.492 (a) (2)) but international search fee paid to USPTO (37 CFR 1.445(a)(2)) .. \$710.00 Neither international preliminary examination fee (37 CFR 1.492 (a) (3)) nor international search fee (37 CFR 1.445(a)(2)) paid to USPTO) \$1000.00 International preliminary examination fee paid to USPTO (37 CFR 1.492 (a) (4)) and all claims satisfied provisions of PCT Article 33(2)-(4) \$100.00 Search Report prepared by the EPO or JPO (37 CFR 1.492 (a) (5)) \$860.00 <div style="text-align: right;">ENTER APPROPRIATE BASIC FEE AMOUNT =</div>				CALCULATIONS		PTO USE ONLY	
Surcharge of \$130.00 for furnishing the oath or declaration later than <input checked="" type="checkbox"/> 20 <input type="checkbox"/> 30 months from the earliest claimed priority date (37 CFR 1.492(e)).				\$ 130.00			
Claims	Number Filed	Number Extra	Rate				
Total Claims	19 - 20 =	-0-	x \$18.00	\$			
Independent Claims	2 - 3 =	-0-	x \$80.00	\$			
Multiple Dependent Claim(s) (if applicable)			+ \$270.00	\$			
TOTAL OF ABOVE CALCULATIONS =				\$	990.00		
Reduction by 1/2 for filing by small entity , if applicable. Verified Small Entity statement must also be filed. (Note 37 CFR 1.9, 1.27, 1.28).				\$			
SUBTOTAL =				\$	990.00		
Processing fee of \$130 for furnishing the English translation later than <input checked="" type="checkbox"/> 20 <input type="checkbox"/> 30 months from the earliest claimed priority date (37 CFR 1.492(f))				\$ 130.00			
TOTAL NATIONAL FEE =				\$	1120.00		
Fee of \$40.00 for recording the enclosed assignment (37 CFR 1.21(h)). Assignment must be accompanied by appropriate cover sheet (37 CFR 3.28, 3.31).				\$			
TOTAL FEES ENCLOSED =				\$	1120.00		
				Amt. to be refunded:		\$	
				Amt. charged:		\$	

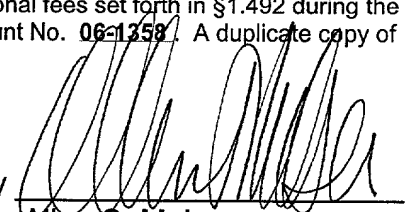
a. ☒ A check in the amount of \$ 1120.00 to cover the above fees is enclosed.

b. ☐ Please charge my Deposit Account No. 06-1358 in the amount of \$ _____ to cover the above fees. A duplicate copy of this sheet is enclosed.

c. ☒ The Commissioner is hereby authorized to charge my account any additional fees set forth in §1.492 during the pendency of this application, or credit any overpayment to Deposit Account No. 06-1358. A duplicate copy of this sheet is enclosed.

SEND ALL CORRESPONDENCE TO:

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By 
 Allen S. Melser
 Reg. No. 27,215

09/869317

Rec'd PCT/PTO 21 DEC 2001

PATENT

IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

In re Application of: :
: Volker GERSTNER et al. :
: U.S. Application No. 09/869,317 : Art Unit: (not yet assigned)
: Internat'l Appl. No. PCT/EP00/11626 :
: Internat'l Appl. Filed: November 22, 2000 : Examiner: (not yet assigned)
: For: METHOD FOR DETECTING : Atty Docket: P66886US0
: FLUORESCENCE PHENOMENA :
: IN MICROSCOPE :
:

PRELIMINARY AMENDMENT

Commissioner for Patents
Washington, D.C. 20231

Sir:

Prior to examination, Applicant submits the following Amendment and Remarks.

It is not believed that extensions of time or fees for net addition of claims are required, beyond those that may otherwise be provided for in documents accompanying this paper. However, in the event that additional extensions of time are necessary, then such extensions of time are hereby petitioned under 37 CFR § 1.136(a); and any fees required for consideration of this paper and any papers associated with it (including fees for net addition of claims) are hereby authorized to be charged to our Deposit Account No. 06-1358.

Kindly enter the following Amendment:

IN THE DRAWINGS

Please amend the drawings as indicated in the accompanying Request For Approval Of Proposed Drawing Corrections.

IN THE SPECIFICATION

Please amend the specification by replacing it with the substitute specification submitted herewith.

IN THE CLAIMS

Amend claims 1-19 as follows:

1. (Amended) A process for detecting the phenomenon of fluorescence in a microscope, comprising the steps of:

irradiating a sample by at least one of a modulated and a pulsed laser light source so as to produce fluorescence, and

detecting the fluorescence with a detector having variable phase positions, at least in two different phase positions of the detector.

2. (Amended) The process, as claimed in claim 1, further comprising the step of generating an image for each phase position using a signal output by the detector.

3. (Amended) The process, as claimed in claim 2, further comprising the step of displaying the image generated for each phase position on a monitor.

4. (Amended) The process, as claimed in claim 1, wherein said steps of irradiating and detecting are carried out using a laser scanning microscope.

5. (Amended) The process, as claimed in claim 1, wherein said detecting step is carried out using a modulatable PMT as the detector.

6. (Amended) A process for detecting the phenomenon of fluorescence in a microscope, comprising the steps of:

irradiating a sample using at least one of a modulated and a pulsed laser light source so as to produce fluorescence,

multiplying a reference signal, corresponding to the at least one of the modulated and pulsed laser, and a measurement signal, corresponding to a modulated detection of the fluorescence, together with a fixed variable phase relation to obtain a result; and

using the result to display an image.

7. (Amended) The process, as claimed in claim 6, wherein the phase relation between the reference signal and the measurement signal is adjusted in such a manner that the phase shift is zero.

8. (Amended) The process, as claimed in claim 6, wherein said detecting step is carried out using non-descanned detection.

9. (Amended) The process, as claimed in claim 1, wherein said irradiating step is carried out using multiphoton excitation of fluorescence emission.

10. (Amended) The process, as claimed in claim 1, wherein said irradiating step is carried out using a cw laser, modulated by means of an acousto-optical modulator (AOM).
11. (Amended) The process, as claimed in claim 1, wherein said irradiating step is carried out using a cw laser, modulated by means of a Pockel cell.
12. (Amended) The process, as claimed in claim 1, wherein said irradiating step is carried out using a pulse laser, which is additionally modulated.
13. (Amended) The process, as claimed in claim 1, wherein said irradiating step is carried out using a pulse laser, which is additionally modulated by means of an acousto-optical modulator.
14. (Amended) The process, as claimed in claim 1, wherein said irradiating step is carried out using a pulse laser, which is additionally modulated by means of a Pockel cell.
15. (Amended) The process, as claimed in claim 1, wherein said detecting step is carried out using time resolution and wherein said irradiating step is carried out using a multiphoton process.

16. (Amended) The process, as claimed in claim 1, wherein said irradiating step is carried out using a pulsed near infrared laser.

17. (Amended) The process, as claimed in claim 1, wherein said irradiating step is carried out using a pulsed near infrared laser, and further comprising the step of:

converting the frequency of the laser downstream to 1 photon excitation.

18. (Amended) The process, as claimed in claim 1, wherein said irradiating step is carried out using a pulsed near infrared laser, and further comprising the step of:

converting the frequency of the laser downstream to 1 photon excitation of fluorescence.

19. (Amended) The process, as claimed in claim 1, wherein said detecting step is carried out using phase sensitive detection for improving the signal to noise ratio.

Please add the following new claims 20-38:

20. (New) The process, as claimed in claim 2, further comprising the step of carrying out a mathematical algorithm on the image to produce another image.

21. (New) The process, as claimed in claim 7, wherein said detecting step is carried out using non-descanned detection.

22. (New) The process, as claimed in claim 1, wherein said irradiating step is carried out using two photon excitation.
23. (New) The process, as claimed in claim 6, wherein said irradiating step is carried out using multiphoton excitation of fluorescence emission.
24. (New) The process, as claimed in claim 6, wherein said irradiating step is carried out using two photon excitation.
25. (New) The process, as claimed in claim 6, wherein said irradiating step is carried out using a cw laser, modulated by means of an acousto-optical modulator.
26. (New) The process, as claimed in claim 6, wherein said irradiating step is carried out using a cw laser, modulated by means of a Pockel cell.
27. (New) The process, as claimed in claim 6, wherein said irradiating step is carried out using a pulse laser, which is additionally modulated.
28. (New) The process, as claimed in claim 6, wherein said irradiating step is carried out using a pulse laser, which is additionally modulated by means of an acousto-optical modulator.

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29. (New) The process, as claimed in claim 6, wherein said irradiating step is carried out using a pulse laser, which is additionally modulated by means of a Pockel cell.

30. (New) The process, as claimed in claim 15, wherein in said irradiating step, the multiphoton process is second harmonic generation on surfaces.

31. (New) The process, as claimed in claim 15, wherein in said irradiating step, the multiphoton process is two photon excitation.

32. (New) The process, as claimed in claim 6, wherein said detecting step is carried out using time resolution and wherein said irradiating step is carried out using a multiphoton process.

33. (New) The process, as claimed in claim 32, wherein in said irradiating step, the multiphoton process is second harmonic generation on surfaces.

34. (New) The process, as claimed in claim 32, wherein in said irradiating step, the multiphoton process is two photon excitation.

35. (New) The process, as claimed in claim 6, wherein said irradiating step is carried out using a pulsed near infrared laser.

36. (New) The process, as claimed in claim 6, wherein said irradiating step is carried out using a pulsed near infrared laser, and further comprising the step of:

converting the frequency of the laser downstream to 1 photon excitation.

37. (New) The process, as claimed in claim 6, wherein said irradiating step is carried out using a pulsed near infrared laser, and further comprising the step of:

converting the frequency of the laser downstream to 1 photon excitation of fluorescence.

38. (New) The process, as claimed in claim 6, wherein said detecting step is carried out using phase sensitive detection for improving the signal to noise ratio.

REMARKS

Claims 20-38 are pending in the application.

By the foregoing Amendment, claims 1-19 are amended as more fully set forth below. New claims 20-38 are added. Pursuant to 37 CFR § 1.121(b)(3), the specification is amended by replacement with a substitute specification in compliance with 37 CFR § 1.125(b). The substitute specification includes no new matter. A marked-up version of the substitute specification showing all changes to the specification of record is submitted herewith. Also attached hereto is a marked-up version of the claims showing the changes made thereto by the current Amendment. The attached page is titled "CLAIMS MARKED TO SHOW CHANGES."

Claims 3, 4, 5, 8, 10, 11, 12, 13, 14, 15, 16, 17, 18, and 19 have been amended to cancel multiple claim dependencies.

Claims 1, 2, 3, 4, 5, 6, 8, 9, 10, 11, 12, 13, 14, 15, 16, 17, 18, and 19 have been amended to recite their subject matter as one or more steps, or as a further limitation of a previously-recited step in a preceding claim, for better conformity with the requirements of U.S. practice.

Claims 1 and 6 have been amended to avoid the use of the alternative recitation "and/or."

Claims 1 and 6 have been amended to supply missing antecedent basis.

It is proposed that the drawings be amended as indicated in the accompanying Request For Approval Of Proposed Drawing Corrections, in order to translate the figure labels, to delete extraneous markings, and to add and/or correct various reference labels.

These changes are believed not to introduce new matter, and entry of the Amendment is respectfully requested.

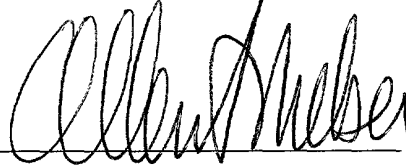
Conclusion

The application is now believed to be in condition for examination and allowance. Should any questions arise, the Examiner is invited to call the undersigned representative so that this case may receive an early Notice of Allowance.

Favorable consideration and allowance are earnestly solicited.

Respectfully submitted,

JACOBSON HOLMAN PLLC

By: 

Date: December 21, 2001

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CLAIMS MARKED TO SHOW CHANGES

In the Claims

Claims 1-19 have been amended as follows:

1. (Amended) [Process] A process for detecting the phenomenon of fluorescence in a microscope, [wherein] comprising the steps of:

irradiating a [the] sample [is irradiated] by at least one of a modulated and [/ or] a pulsed laser light source so as to produce fluorescence, and

detecting the fluorescence [is detected] with a detector having variable phase positions, at least in two different phase positions of the detector.

2. (Amended) [Process] The process, as claimed in claim 1, [wherein] further comprising the step of generating an image [is produced] for each phase position using a signal output by the detector.

3. (Amended) [Process] The process, as claimed in [at least one of the preceding claims, wherein the generated images or the images, calculated from these images, are displayed] claim 2, further comprising the step of displaying the image generated for each phase position on a monitor.

4. (Amended) [Process] The process, as claimed in [at least one of the preceding claims] claim 1, wherein [the illumination and the detection take place by way of] said steps of irradiating and detecting are carried out using a laser scanning microscope.

5. (Amended) [Process] The process, as claimed in [at least one of the preceding claims] claim 1, wherein [the detection takes places with] said detecting step is carried out using a modulatable PMT as the detector.

6. (Amended) [Process] A process for detecting the phenomenon of fluorescence in a microscope, [wherein] comprising the steps of:

irradiating a [the] sample [is irradiated by] using at least one of a modulated and [/ or] a pulsed laser light source so as to produce fluorescence,

[wherein] multiplying a reference signal, corresponding to the at least one of the modulated and [/ or] pulsed laser, and a measurement signal, corresponding to a modulated detection of the fluorescence, [are multiplied] together with a fixed variable phase relation to obtain a result; and

[the result serves] using the result to display [the] an image.

7. (Amended) [Process] The process, as claimed in claim 6, wherein the phase relation between the reference signal and the measurement signal is adjusted in such a manner that the phase shift is zero.

8. (Amended) [Process] The process, as claimed in [any of the claims 6 or 7] claim 6, [with] wherein said detecting step is carried out using non-descanned detection.

9. (Amended) [Application of a process, according to any one of the preceding claims, to the]
The process, as claimed in claim 1, wherein said irradiating step is carried out using multiphoton
excitation of fluorescence emission[, in particular two photon excitation].

10. (Amended) [Process] The process, as claimed in [any one of the preceding claims, with the
use of] claim 1, wherein said irradiating step is carried out using a cw laser, modulated by means of
an acousto-optical modulator (AOM).

11. (Amended) [Process] The process, as claimed in [any one of the preceding claims, with the
use of] claim 1, wherein said irradiating step is carried out using a cw laser, modulated by means of
a Pockel cell.

12. (Amended) [Process] The process, as claimed in [any one of the preceding claims, with the
use of] claim 1, wherein said irradiating step is carried out using a pulse laser, which is additionally
modulated.

13. (Amended) [Process] The process, as claimed in [any one of the preceding claims, with the
use of] claim 1, wherein said irradiating step is carried out using a pulse laser, which is additionally
modulated by means of an [AOM] acousto-optical modulator.

14. (Amended) [Process] The process, as claimed in [any one of the preceding claims, with the use of] claim 1, wherein said irradiating step is carried out using a pulse laser, which is additionally modulated by means of a Pockel cell.

15. (Amended) [Process] The process, as claimed in [any one of the preceding claims] claim 1, [for use for] wherein said detecting step is carried out using time resolution [of] and wherein said irradiating step is carried out using a multiphoton [processes, like second harmonic generation on surfaces or two photon excitation] process.

16. (Amended) [Process] The process, as claimed in [any one of the preceding claims, with the use of] claim 1, wherein said irradiating step is carried out using a pulsed near infrared [(NIR)] laser.

17. (Amended) [Process] The process, as claimed in [any one of the preceding claims, with the use of] claim 1, wherein said irradiating step is carried out using a pulsed near infrared [(NIR)] laser, and further comprising the step of:

[with] converting the frequency of the laser downstream [frequency conversion] to 1 photon excitation.

18. (Amended) [Process] The process, as claimed in [any one of the preceding claims, with the use of] claim 1, wherein said irradiating step is carried out using a pulsed near infrared [(NIR)] laser, and further comprising the step of:

[with] converting the frequency of the laser downstream [frequency conversion] to 1 photon excitation of fluorescence.

19. (Amended) [Process] The process, as claimed in [any one of the preceding claims, with the use of] claim 1, wherein said detecting step is carried out using phase sensitive detection for improving the signal to noise ratio.

New claims 20-29 have been added as follows:

--20. The process, as claimed in claim 2, further comprising the step of carrying out a mathematical algorithm on the image to produce another image.

--21. The process, as claimed in claim 7, wherein said detecting step is carried out using non-descanned detection.

--22. The process, as claimed in claim 1, wherein said irradiating step is carried out using two photon excitation.

--23. The process, as claimed in claim 6, wherein said irradiating step is carried out using multiphoton excitation of fluorescence emission.

--24. The process, as claimed in claim 6, wherein said irradiating step is carried out using two photon excitation.

--25. The process, as claimed in claim 6, wherein said irradiating step is carried out using a cw laser, modulated by means of an acousto-optical modulator.

--26. The process, as claimed in claim 6, wherein said irradiating step is carried out using a cw laser, modulated by means of a Pockel cell.

--27. The process, as claimed in claim 6, wherein said irradiating step is carried out using a pulse laser, which is additionally modulated.

--28. The process, as claimed in claim 6, wherein said irradiating step is carried out using a pulse laser, which is additionally modulated by means of an acousto-optical modulator.

--29. The process, as claimed in claim 6, wherein said irradiating step is carried out using a pulse laser, which is additionally modulated by means of a Pockel cell.

--30. The process, as claimed in claim 15, wherein in said irradiating step, the multiphoton process is second harmonic generation on surfaces.

--31. The process, as claimed in claim 15, wherein in said irradiating step, the multiphoton process is two photon excitation.

--32. The process, as claimed in claim 6, wherein said detecting step is carried out using time resolution and wherein said irradiating step is carried out using a multiphoton process.

--33. The process, as claimed in claim 32, wherein in said irradiating step, the multiphoton process is second harmonic generation on surfaces.

--34. The process, as claimed in claim 32, wherein in said irradiating step, the multiphoton process is two photon excitation.

--35. The process, as claimed in claim 6, wherein said irradiating step is carried out using a pulsed near infrared laser.

--36. The process, as claimed in claim 6, wherein said irradiating step is carried out using a pulsed near infrared laser, and further comprising the step of:

converting the frequency of the laser downstream to 1 photon excitation.

--37. The process, as claimed in claim 6, wherein said irradiating step is carried out using a pulsed near infrared laser, and further comprising the step of:

converting the frequency of the laser downstream to 1 photon excitation of fluorescence.

--38. The process, as claimed in claim 6, wherein said detecting step is carried out using phase sensitive detection for improving the signal to noise ratio.--

TOP SECRET

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SUBSTITUTE SPECIFICATION

Process for the Detection of the Phenomenon of Fluorescence
in a Microscope

BACKGROUND OF THE INVENTION

Field of the Invention

[0001] The process that is presented relates to confocal and 2-photon fluorescence microscopy as described by M. Göppert-Mayer, Ann. Physik 9, 273 (1931) and T. Wilson, *Theory and Practice of Scanning Optical Microscopy* (Academic Press, 1984). Both methods are assumed to be known.

[0002] Both confocal fluorescence microscopy and 2-photon microscopy are modified by the method described below to the extent that an additional contrast parameter is possible: the fluorescence lifetime.

Related Art

[0003] Temporal resolved fluorescence and/or the use of the lifetime as a contrast parameter in confocal/2-photon microscopy can be carried out by two different methods - by time domain detection and frequency domain detection.

[0004] In the case of time domain detection (described in Published patent application DE 41 04 014 of Wabnitz, entitled "Method for Determining the Calcium Concentration in Cells"; and in Patent DE 36 14 359 C2 of Gröbler, entitled "Device for the Analysis and Imaging of Real Time Intensity of Fluorescence Radiation resulting from Point-by-Point Excitation of a Preparation by

means of Laser Light”) a fluorescent sample is excited so as to produce fluorescence by means of a pulsed light source, and the fluorescence emission is detected with time resolution either by means of time correlated single photon counting (TCSPC) (described in Patent WO 98 / 09154 to Müller et al., entitled “System for Differentiating Fluorescing Molecular Groups by means of Time-Resolved Fluorescence Measurement”; and in Published patent application DE 42 31 477 A1 of Han, entitled “Method for Optical Sorting of Plastics by means of Time-Resolved Laser Spectroscopy”) or by means of time gated detection (described by H. Schneckenburger et al., “Time-Gated H. Microscopic Imaging and Spectroscopy in Medical Diagnosis and Photobiology,” *Optical Engineering* 33 (8) 2600 (1994); R. Cubeddu et al., “A Real Time System for Fluorescence Lifetime Imaging,” *SPIE* 2976 (1997) 98; and K. Dowling et al., “Two Dimensional Fluorescence Lifetime Imaging using a 5 kHz / 110 ps Gated Image Intensifier” (www.kentech.co.uk/pdf_files/K_Dowling_et_al.pdf)).

[0005] In the case of frequency domain detection, a fluorescent sample or preparation is excited with a light source that is either actively modulated or pulsed (for example, by means of passive mode coupling). Since any arbitrary modulation of the excitation by means of a Fourier analysis breaks down into sinusoidal components, the observation of a sinusoidal excitation is adequate. The frequency domain detection technique is based on the delay of the fluorescence emission by a phase ϕ and a change in the modulation depth M compared with the excitation light as a function of the modulation frequency $\omega (= 2\pi f_{\text{mod}})$ and the lifetime τ .

$$\phi = a \tan(\omega\tau) \quad (1)$$

$$M = \frac{1}{\sqrt{1 + \omega^2 \tau^2}} \quad (2)$$

[0006] However, the resulting fluorescence signal, oscillated with the modulation frequency, is out of phase and demodulated. For typical fluorescence lifetimes ranging from $\tau = 1...10$ ns, modulation frequencies ranging from $f_{mod} = 10...100$ MHz are adequate.

[0007] Since it generally does not make any sense to scan the fluorescence signal at such high modulation frequencies, a frequency mixing process is used to detect the signal. For mixing, any detection element with a modulatable amplification is suitable.

[0008] In essence two methods are distinguished - the homodyne and the heterodyne detection techniques.

[0009] To understand the principle, one observes generally two "signals" S_1 , S_2 , (where, for example S_1 is modulated excitation, and S_2 is modulated amplification).

$$\begin{aligned} S_1 &= A_0 + A_1 \cos(\omega_a t + \alpha) \\ S_2 &= B_0 + B_1 \cos(\omega_b t + \beta) \end{aligned} \quad (3)$$

Multiplication results in:

$$\begin{aligned} S_1 S_2 &= A_0 B_0 + A_0 B_1 \cos(\omega_b t + \beta) + B_0 A_1 \cos(\omega_a t + \alpha) + \\ &A_1 B_1 \left\{ \cos((\omega_a \omega_b)t + (\alpha + \beta)) + \cos((\omega_a \omega_b)t + (\alpha - \beta)) \right\} \end{aligned} \quad (4)$$

Homodyne Detection

[00010] If $\omega_a = \omega_b$ (homodyne), the second harmonic and a frequency independent component are generated by the mixing process of the "signals" S_1 and S_2 . A low pass filter results in a suppression of the components at ω_a and $2\omega_a$. Only the DC background and the phase dependent DC component are detected. The signal, filtered by means of a low pass (LP) filter, can be written as:

$$LP(S_1 S_2) = A_0 B_0 + A_1 B_1 \cos(\alpha - \beta) \quad (5)$$

[00011] In the case of homodyne detection this frequency independent (DC) signal can be detected in multiple relative phases. To measure the fluorescence lifetime, at least 3 three different phase positions are necessary. At just two relative phase positions, the phase shift or the demodulation, induced by the fluorescence lifetime, can be used as the contrast parameter (as described by P.C. Schneider et al., "Rapid Acquisition, Analysis and Display of Fluorescence Lifetime Resolved Images for Real time Applications," *Rev. Sci. Instrum.* 68 (11) 4107 (1997) (hereafter, "Schneider et al.")).

Heterodyne Detection - Cross Correlation

[00012] If $\omega_b = \omega_a + D\omega$ (heterodyne), the mixing process generates a high frequency signal at the total frequency and a signal at the cross correlation frequency $\Delta\omega$. Again the high frequency components are suppressed by a low pass filter.

$$LP(S_1 S_2) = A_0 B_0 + A_1 B_1 \cos(\Delta\omega t + \alpha - \beta) \quad (6)$$

[00013] In the case of heterodyne detection, the differential frequency $\Delta\omega$ is detected. Phase position and modulation depth of the signal at the differential frequency make it possible to determine the lifetime. Typical cross correlation frequencies range from a few Hz up to about 100 kHz.

[00014] A more comprehensive presentation of the heterodyne method can be found in the publication by E. Gratton et al., "A Continuously Variable Frequency Cross Correlation Phase Fluorometer with Picosecond Resolution," *Biophys. J.* 44 (1983) 315 (hereinafter, "Gratton"), and

"Multifrequency Phase and Modulation Fluorometry," *Ann. Rev. Biophys. Bioeng.* 13 (1984) 105 (hereinafter, "Gratton 2").

[00015] In both the homodyne and heterodyne detection technique the high frequency change is reflected, so to speak, on the low frequency range.

[00016] Owing to the multi-exponential decay behavior of the fluorescence emission, the lifetimes, determined from the modulation depth and the phase shift, vary. Therefore, for precise measurement of the lifetime, the excitation frequency has to be varied as described by Gratton 2.

[00017] If, in contrast, the lifetime is supposed to be used, for example, as a contrast parameter in an imaging process, this is generally not necessary. Frequently it suffices, for example, to show the phase shift or the demodulation by means of the lifetime or by means of the lifetime, calculated from the phase shift and demodulation data, at a fixed modulation frequency.

BRIEF DESCRIPTION OF THE DRAWINGS

[00018] The invention is better understood by reading the following Detailed Description of the Preferred Embodiments with reference to the accompanying drawing figures, in which like reference symbols refer to like elements throughout, and in which:

[00019] Figure 1 is a schematic diagram showing apparatus for detecting fluorescence in a microscope in accordance with the present invention.

[00020] Figure 2 is a schematic diagram showing a scan unit and a non-descanned detection unit.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

1.1 One Photon Confocal Lifetime Imaging, Homodyne

[00021] The confocal design of a laser scanning microscope (LSM) is modified for lifetime imaging to the extent that

- the excitation light source is modulated or a pulse laser is used.
- the amplification of the detector (for example, a photomultiplier tube (PMT)) is modified.
- an electronic phase shifter is used that permits the relative phase position of light excitation and detection to be adjusted. This circuit with the components that are used is shown in Figure 1.

First Embodiment

[00022] Driven by means of a synthesizer S using a quartz crystal, RF frequencies are generated in the range from 10 to 100 MHZ. The output of the synthesizer S is connected, on the one hand, over a shielded high frequency line (for example, over a BNC cable) to a phase shifter/amplifier PA. The phase shifter/amplifier PA amplifies, on the one hand, the high frequency input signal of the synthesizer - in the first embodiment, to a power of approximately 1.5 W at a resistance of 50W. Furthermore, the phase position of the amplified RF signal can be varied with the phase shifter/amplifier PA. The relative phase of the phase shifter/amplifier PA can be adjusted digitally over a control line, for example, by means of a control via a serial interface of a PC. The amplified RF signal is fed to a modulated PMT, designated PMT1 in Figure 1 - for example, the PMT module (H 6573) of Hamamatsu, the "Technical Information" for which contains a detailed presentation of the operating mode. The amplified RF voltage (approximately $25 V_{pp} / 50W$) is fed

in the PMT to the second dynode and used to modulate the amplification of the PMT. To produce a defined low pass filter, the output signal of the PMT can be smoothed by means of a commercial low pass (LP) filter LPF. The 3 dB threshold frequency f_g of the LP filter LPF is selected in such a manner that

$$1 / \text{pixel dwell time} \ll f_g \ll f_{\text{laser}}$$

where f_{laser} = the laser modulation frequency. The signal filtered thus is fed to the standard detection electronics of the laser raster microscope (LRM). (For greater comprehension: in principle, for example, to an ADC (analog digital converter), which is synchronized with the xy scanners XYs of the LRM.

[00023] A second identical output of the synthesizer S is also connected to the control electronics CE of the light modulator M by means of a high frequency line L. An acousto-optical modulator (or an electro-optical modulator) can be used, for example, as the modulator M in the laser beam path. The light modulator M is a component of the laser module of the confocal laser raster microscope. Such a design makes it possible to vary the relative phase position of the phase shifter/amplifier PA and the light modulator M. The frequencies for the light modulator M for modulating the laser light and the PMT amplification voltage are identical. The phase position generally varies. At least the phase of an RF output can be adjusted digitally in about 1° steps. In the case depicted in Figure 1, the phase of the PMT modulation voltage is varied in the phase shifter/amplifier PA by means of the phase shifter.

[00024] The operating mode and the related advantages of the method in accordance with the first embodiment will now be described.

[00025] Using the conventional LSM design, the light of the modulated/pulsed laser light source is focused on the lens plane by means of the scan mirrors and the LSM scan optics. The fluorescence is focused, as in the confocal Zeiss LSM510, in the direction of reflection on the detection pin hole using a beam splitter, focusing lens, etc. The raster-shaped movement of the laser focus over the lens plane and the synchronized detection - in the now modulated - PMT result in a confocal image of the lens plane. By using the homodyne technique, the PMT signal at the output of the LP filter LPF (image 1) is a DC signal, which varies only as a function of the laser spot position (pixel). Through repeated scanning operations during multiple different relative phases of the light modulator and detection modulation, it is possible to detect the fluorescence lifetime contrast or to measure the fluorescence lifetime. The significant advantage lies in the fact that the conventional data acquisition unit of the LRM can be used. The lifetime contrast is calculated from image to image.

[00026] Image digitizing to produce the lifetime contrast in a confocal microscope image and/or to display the confocal lifetime distribution of dyes is carried out in accordance with the following steps.

[00027] In a first step in the embodiment presented here, a first phase of the PMT detector PMT1 is adjusted digitally. The adjustment is done, as described above, with the electronic phase shifter/amplifier PA; and the resulting DC signal of the PMT (following the usual conversion from current to voltage and the usual conversion from analog to digital) is registered by means of the usual (LSM) analysis electronics in synchronism synchronization with the scanner XYS and stored in the PC by means of a storage medium.

[00028] In at least a second step the process is repeated with a second different relative phase position.

[00029] The at least two digital images are displayed, for example, by means of a computer screen without any further calculation.

[00030] For the presentation, images, generated with the following Fourier expansion algorithms, are also displayed on the screen :

[00031] The Fourier expansion is expressed by

$$I(\varphi + \varphi_\tau) = a_0 + a_1 \cdot \sin(\varphi) + b_1 \cdot \cos(\varphi) \quad (7)$$

with the fluorescence intensity of a pixel I and the corresponding Fourier coefficients a_0, a_1, b_1 , where.

$$a_0 = \bar{I} = \frac{1}{N} \sum_{n=0}^{N-1} I\left(\varphi_\tau + n \frac{2\pi}{N}\right)$$

$$a_1 = \frac{2}{N} \sum_{n=0}^{N-1} \sin\left(\frac{2\pi n}{N}\right) I\left(\varphi_\tau + \frac{2\pi n}{N}\right) \quad (8)$$

$$b_1 = \frac{2}{N} \sum_{n=0}^{N-1} \cos\left(\frac{2\pi n}{N}\right) I\left(\varphi_\tau + n \frac{2\pi}{N}\right)$$

[00032] At the same time a_0, a_1, b_1 are the Fourier coefficients (per pixel), $N \geq 2$ the number of the stored phase images (or pixel intensity) $I = I(\phi)$.

[00033] The modulation depth M_τ and the phase shift can be expressed by the lifetime ϕ_τ using the Fourier coefficients.

$$M_\tau = \frac{\sqrt{a_1^2 + b_1^2}}{a_0} = \frac{1}{\sqrt{1 + \omega^2 \tau^2}} \quad (9)$$

$$\phi_\tau = -1 \cdot \frac{a_1}{b_1} = \omega \tau \quad (10)$$

[00034] The modulation depth M is calculated pixel by pixel. $M = M(i, j) = M_{ij}$, (i, j , pixel indices). Similarly the phase shift $\phi = \phi(i, j) = \phi_{ij}$.

[00035] The image of the modulation depth M_{ij} , which is calculated pixel by pixel in this manner, and the phase shift ϕ_{ij} , are displayed on the monitor.

[00036] Another type of display is the τ imaging, that is the lifetime $\tau(M)_{ij}$ or $\tau(\phi)_{ij}$, calculated for τ by means of resolution equations (9) or (10), as described by Schneider et al.

$$\tau(M) = \frac{1}{\omega} \cdot \sqrt{\frac{1}{M^2} - 1} \quad (11)$$

$$\tau(\phi) = \frac{1}{\omega} \tan(\phi) \quad (12)$$

[00037] M and ϕ are calculated with the equation (9) or (10); and the Fourier coefficients a_0 , a_1 , b_1 , determined with equation (8), are calculated.

[00038] To increase the accuracy in determining the phase, it is also possible to use the optimized algorithm, presented in a paper, "Phase Evaluation by Folding," by Küchel, 1989.

Second Embodiment:

[00039] Another embodiment of a confocal microscope with lifetime contrast or for the measurement of the lifetime distribution in a confocal split image can be achieved using pulse lasers. Suitable are, for example, pulse laser diodes or other, for example femtosecond (fs) laser systems (for example, a Ti:sapphire laser), for example with a downstream frequency conversion unit (for example, frequency doubling, tripling). When pulse lasers are used, there is no need to generate the RF driver frequency with synthesizers. Instead, an electronic diode signal of the pulse laser is provided (for example, PD signal out of the fs/ps NIR laser in Figure 1 or an equivalent construction with exchange/expansion of the VIS laser module, for example with a ps diode laser etc.). The resulting RF signal of the (sufficiently fast) photodiode is a priori synchronized with the laser excitation. The RF signal can be used analogously with the RF signal of a synthesizer. That is, the phase shifter/amplifier PA is made available at the corresponding input (by way of an RF line). The rest of the process is analogous to that of the first embodiment. What is advantageous here is, on the one hand, the use of a pulse-shaped light source and the associated improvement of the signal-to-noise ratio in a lifetime contrast, generated thereby, as compared to the sinusoidal modulation of the laser excitation in the first embodiment and, on the other hand, the omission of a synthesizer for generating the RF frequency. The fluorescence is detected after a 1 photon excitation (linear in the excitation intensity).

1.2 Two Photon Confocal Lifetime Imaging, Homodyne

[00040] A third embodiment, using the combination of 2-photon microscopy with the homodyne detection technique for lifetime imaging, will now be described.

[00041] The combination of time resolution and 2-photon microscopy was already demonstrated by Gratton with the so called heterodyne technique, as described by So et al., "Time Resolved Fluorescence Microscopy using Two Photon Excitation," *Bioimaging* 3 (1995) 49 (hereinafter, "So et al."). In the heterodyne technique an fs laser is used for fluorescence excitation in a 2-photon microscope; and the PMT detector is driven at a slightly different modulation frequency. The typical repetition rate of fs Ti:sapphire lasers is in the 80 MHz range. In the So et al. article, a frequency of 80 MHz + 25 kHz is used for amplification modulation of the PMT detector. The consequence is a beat. This beat is digitized with an analog to digital conversion (ADC) card and scanned. Thus, it is possible to detect pixel by pixel the phase shift from excitation to fluorescence (heterodyne method).

[00042] In the design in accordance with the present invention, the phase shift is determined, compared to that described by So et al., not pixel by pixel, but rather image by image. That is, first one image is captured during a relative phase shift ϕ_1 and stored. In at least one other step, an image is generated during another different relative phase ϕ_2 (homodyne method).

[00043] The diverse images for presenting the contrast are calculated in the same manner as described above in connection with the one-photon homodyne detection technique for confocal lifetime imaging.

[00044] The procedure by which 2-photon microscopy is combined with the homodyne detection technique for lifetime imaging will now be described.

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[00045] A dyed or self-fluorescing sample is excited so as to emit fluorescence by way of two photon absorption. The pulsed laser can be, for example, a Ti:sapphire laser (also sums with double or triple frequency or a difference with mixed frequency, etc.), a ps laser diode or a laser, which is modulated, for example, by means of an optical modulator M, such as an acousto-optical modulator (AOM) or an electro-optical modulator (EOM). In the first and second embodiments, the physical process is a one photon excitation; in the third embodiment, it is two photon excitation (or in general multiphoton excitation). To excite the fluorescence in the embodiment according to Figure 1, an fs Ti:sapphire laser is used. The repetition rate of the fs laser is approximately 80 MHz, non-linear optics laser scanning microscope (NLO - LSM), fluorescence detection method).

[00046] For detection, a modulatable PMT detector from Hamamatsu (H6573) is used. The sinusoidal modulation frequency is generated from a photodiode signal of the laser (fs Mira, Coherent Corporation) by way of an emitter coupled logic (ECL) logic circuit and amplified to an average power of 15.W at 50W by means of an RF amplifier, integrated into the phase shifter/amplifier PA, and is available at the output "RF out" of the PA. The phase of the generated sine (and thus the amplified sine) can be adjusted to approximately 1° (analogous to the first and second embodiments). The electronic jitter is < 100 ps ((Figure 1), phase shifter/RF amplifier). With the amplified sine wave at the frequency, corresponding to the laser repetition rate ($f_{rep} = f_{mod}$), the amplification of the PMT detector is modulated. To this end, the amplified RF frequency is made available to the input of the PMT module, called "RF modulation in" in Figure 1. The current at the output of the PMT detector is smoothed with a passive LP filter or is integrated by a different method by way of the integration circuit. The resulting DC signal is made available again to the

detection unit of an LRM. The rest of the procedure for gathering and evaluating the data is analogous to that described in connection with the first and second embodiments.

[00047] The distinction with respect to the first and second embodiments lies in the fact that in one case a two photon (NLO) LSM is combined with the lifetime imaging. That is, the fluorescence excitation occurs with an fs or ps pulse laser. Thus, another significant difference is the type of fluorescence excitation (here two or generally multiphotons (> 2) excitation).

1.3 Arrangement for Phase Sensitive Fluorescence Detection in a Laser Scanning Microscope

[00048] For two or multiphoton excitation, it is possible to use more efficient detection units due to the depth discriminated excitation. They are described in the literature under the collective term of non-descanned detection units.

[00049] This detection unit is shown in Figure 2 as a schematic drawing, which is attached to the scan lens SL and the scanner XY of Figure 1 and depicts a microscope beam path, with the sample P, the lens OL, the beam splitter ST for coupling in the illumination/coupling out the radiation, coming from the sample, as well as a first tube lens TL1.

[00050] By way of a second tube lens TQ, another modulatable PMT, designated PMT2 in Figure 2, is used for direct detection in a detection beam path DE, that is, not by way of a scan beam path.

[00051] This PMT is connected to the control unit CU in Figure 1 and by way of said control unit CU to other units in Figure 1.

[00052] A significant drawback with these detection units is generally their higher sensitivity to room light. Since the room light is generally not modulated, or is modulated differently from

excitation light, the use of phase sensitive detection units for suppressing the room light is logical. Thus, there is no need for an expensive encapsulation of the detection unit. The configurations for one and two or multiphoton excitation have already been described above and are totally transferable to a phase sensitive detector. However, in the phase sensitive detection technique the reference signal (excitation light) and the measurement signal (fluorescence signal) have the same modulation. For most of the TiSa laser systems that are used, this modulation is 80 MHz. Thus, homodyne detection takes place. For phase sensitive detection, both signals are multiplied together in a multiplier with a fixed variable phase relation. In an advantageous arrangement the first dynode of a modulatable photomultiplier (H6573) functions as the multiplier.

[00053] The reference signal is generated from the above described phase shifter/RF amplifier PA. The clock for the phase shifter is the photodiode signal of the pulse laser. In addition, the repetition rate, predetermined by means of the pulse laser, can be expanded to a variable beat frequency range by "beating" the laser light with an optical modulator M (see Figure 1). The beat frequency is provided by means of a synthesizer with variable phase, which is controlled by means of trigger signals of the excitation light source (see Figure 1). The phase relation between the reference signal and the measurement signal is adjusted in such a manner that the phase shift is zero. Thus, the variable is demodulated. In this manner a DC or low frequency modulated measurement signal is obtained. However, disturbances, like room light, are highly modulated after the multiplier (like the reference signal approx. 80 MHz). Due to the downstream low pass filter the highly modulated portions (disturbances) are filtered out and thus suppressed. An example of the low pass filter is the detection electronics of a conventional LSM.

[00054] The advantage of the described arrangement lies in the fact that the electronics on the detection side has to be designed only for low frequency signals, since the demodulation takes place in the photomultiplier.

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MARKED-UP VERSION OF SUBSTITUTE SPECIFICATION

Process for the Detection of the Phenomenon of Fluorescence
in a Microscope

BACKGROUND OF THE INVENTION

Field of the Invention

[0001] The process that is presented relates to confocal and 2-photon fluorescence microscopy [Goeppert] [Wilson] as described by M. Göppert-Mayer, *Ann. Physik* 9, 273 (1931) and T. Wilson, *Theory and Practice of Scanning Optical Microscopy* (Academic Press, 1984). Both methods are assumed to be known.

[0002] Both confocal fluorescence microscopy and 2-photon microscopy are modified by the method ~~presented~~ described below to the extent that an additional contrast parameter is possible: the fluorescence lifetime.

Related Art

[0003] Temporal resolved fluorescence and/or the use of the lifetime as a contrast parameter in confocal/2-photon microscopy can be carried out by two different methods - by time domain detection and frequency domain detection.

[0004] In the case of time domain detection [Wabnitz] [Gröbler] (described in Published patent application DE 41 04 014 of Wabnitz, entitled "Method for Determining the Calcium Concentration in Cells"; and in Patent DE 36 14 359 C2 of Gröbler, entitled "Device for the Analysis and Imaging of Real Time Intensity of Fluorescence Radiation resulting from Point-by-Point

Excitation of a Preparation by means of Laser Light") a fluorescent sample is excited so as to produce fluorescence by means of a pulsed light source, and the fluorescence emission is detected with time resolution either by means of time correlated single photon counting (TCSPC) [Müller] [Han] (described in Patent WO 98 / 09154 to Müller et al., entitled "System for Differentiating Fluorescing Molecular Groups by means of Time-Resolved Fluorescence Measurement"; and in Published patent application DE 42 31 477 A1 of Han, entitled "Method for Optical Sorting of Plastics by means of Time-Resolved Laser Spectroscopy") or by means of time gated detection [Schbg] [Cubeddu] [Dowling] (described by H. Schneckenburger et al., "Time-Gated H. Microscopic Imaging and Spectroscopy in Medical Diagnosis and Photobiology," *Optical Engineering* 33 (8) 2600 (1994); R. Cubeddu et al., "A Real Time System for Fluorescence Lifetime Imaging," *SPIE* 2976 (1997) 98; and K. Dowling et al., "Two Dimensional Fluorescence Lifetime Imaging using a 5 kHz / 110 ps Gated Image Intensifier" (www.kentech.co.uk/pdf_files/K_Dowling_et_al.pdf)).

[0005] In the case of frequency domain detection, a fluorescent sample or preparation is excited with a light source that is either actively modulated or pulsed (for example, by means of passive mode coupling). Since any arbitrary modulation of the excitation by means of a Fourier analysis falls part breaks down into sinusoidal components, the observation of a sinusoidal excitation is adequate. The frequency domain detection technique is based on the delay of the fluorescence emission by a phase ϕ and a change in the modulation depth M compared with the excitation light as a function of the modulation frequency $\omega (= 2\pi f_{\text{mod}})$ and the lifetime τ .

$$\phi = a \tan(\omega\tau) \quad (1)$$

$$M = \frac{1}{\sqrt{1 + \omega^2 \tau^2}} \quad (2)$$

[0006] However, the resulting fluorescence signal, oscillated with the modulation frequency, is out of phase and demodulated. For typical fluorescence lifetimes ranging from $\tau = 1...10$ ns, modulation frequencies ranging from $f_{\text{mod}} = 10...100$ MHz are adequate.

[0007] Since it generally does not make any sense to scan the fluorescence signal at such high modulation frequencies, a frequency mixing process is used to detect the signal. For mixing, any detection element with a modulatable amplification is suitable.

[0008] In essence two methods are distinguished - the homodyne and the heterodyne detection techniques.

[0009] To understand the principle, one observes generally two “signals” S_1 , S_2 , (where, for example S_1 is modulated excitation, and S_2 is modulated amplification).

$$S_1 = A_0 + A_1 \cos(\omega_a t + \alpha)$$

$$S_2 = B_0 + B_1 \cos(\omega_b t + \beta) \quad (3)$$

Multiplication results in:

$$S_1 S_2 = A_0 B_0 + A_0 B_1 \cos(\omega_b t + \beta) + B_0 A_1 \cos(\omega_a t + \alpha) + A_1 B_1 \left\{ \cos((\omega_a \omega_b)t + (\alpha + \beta)) + \cos((\omega_a \omega_b)t + (\alpha - \beta)) \right\} \quad (4)$$

Homodyne Detection

[00010] If $\omega_a = \omega_b$ (homodyne), the second harmonic and a frequency independent component are generated by the mixing process of the “signals” S_1 and S_2 . A low pass filter results in a

suppression of the components at ω_a and $2\omega_a$. Only the DC background and the phase dependent DC component are detected. The signal, filtered by means of a low pass (~~LP=low pass~~) (LP) filter, can be written as:

$$LP(S_1 S_2) = A_0 B_0 + A_1 B_1 \cos(\alpha - \beta) \quad (5)$$

[00011] In the case of homodyne detection this frequency independent (DC) signal can be detected in multiple relative phases. To measure the fluorescence lifetime, at least 3 three different phase positions are necessary. At just two relative phase positions, the phase shift or the demodulation, induced by the fluorescence lifetime, can be used as the contrast parameter (as described by P.C. Schneider et al., "Rapid Acquisition, Analysis and Display of Fluorescence Lifetime Resolved Images for Real time Applications," Rev. Sci. Instrum. 68 (11) 4107 (1997) (hereafter, "Schneider et al.")) [Clegg].

Heterodyne Detection - Cross Correlation

[00012] If $\omega_b = \omega_a + \Delta\omega$ (heterodyne), the mixing process generates a high frequency signal at the total frequency and a signal at the cross correlation frequency $\Delta\omega$. Again the high frequency components are suppressed by a low pass filter.

$$LP(S_1 S_2) = A_0 B_0 + A_1 B_1 \cos(\Delta\omega t + \alpha - \beta) \quad (6)$$

[00013] In the case of heterodyne detection, the differential frequency $\Delta\omega$ is detected. Phase position and modulation depth of the signal at the differential frequency make it possible to determine the lifetime. Typical cross correlation frequencies range from a few Hz up to about 100 kHz.

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[00016] Owing to the multi-exponential decay behavior of the fluorescence emission, the lifetimes, determined from the modulation depth and the phase shift, vary. Therefore, for precise measurement of the lifetime, the excitation frequency has to be varied [Gratton2] as described by Gratton 2.

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- the excitation light source is modulated or a pulse laser is used.
- the amplification of the detector (for example, ~~PMT~~ a photomultiplier tube (PMT)) is modified.
- an electronic phase shifter is used that permits the relative phase position of light excitation and detection to be adjusted. This circuit with the components that are used is shown in Figure 1.

~~Realization 1:~~ First Embodiment

[00022] Driven by means of a synthesizer S using a quartz crystal, RF frequencies are generated in the range from 10 to 100 MHz. The output of the synthesizer S is connected, on the one hand, over a shielded high frequency line (for example, over a BNC cable) to a phase shifter/amplifier PA. The phase shifter/amplifier PA amplifies, on the one hand, the high frequency input signal of the synthesizer - in the ~~presented realization~~ first embodiment, to a power of ~~approx.~~ approximately 1.5 W at a resistance of 50W. Furthermore, the phase position of the amplified RF signal can be varied with the phase shifter/amplifier PA. The relative phase of the phase

shifter/amplifier PA can be adjusted digitally over a control line, for example, by means of a control via a serial interface of a PC. The amplified RF signal is fed to a modulated PMT, designated PMT1 in Figure 1 [~~=photomultiplier tube~~] - for example, the PMT module (H 6573) ~~from of~~ Hamamatsu, the “Technical Information” for which contains a detailed presentation of the operating mode.⁺ The amplified RF voltage (approximately $25 V_{pp} / 50W$) is fed in the PMT to the second dynode and used to modulate the amplification of the PMT. To produce a defined low pass filter, the output signal of the PMT can be smoothed by means of a commercial low pass (LP) filter LPF. The 3 dB threshold frequency f_g of the LP filter LPF is selected in such a manner that

$$1 / \text{pixel dwell time} \ll f_g \ll f_{laser}$$

where f_{laser} = the laser modulation frequency. The signal filtered thus is fed to the standard detection electronics of the ~~LRM~~ [~~= laser raster microscope~~] laser raster microscope (LRM). (For greater comprehension: in principle, for example, to an ADC (analog digital converter), which is synchronized with the xy scanners XYS of the LRM.

[00023] A second identical output of the synthesizer S is also connected to the control electronics CE of the light modulator M by means of a high frequency line L. An acousto-optical modulator (or an electro-optical modulator) can be used, for example, as the modulator M in the laser beam path. The light modulator M is a component of the laser module of the confocal laser raster microscope. Such a design makes it possible to vary the relative phase position of the phase shifter/amplifier PA and the light modulator M. The frequencies for the light modulator M for modulating the laser light and the PMT amplification voltage are identical. The phase position

⁺ The “Technical Information” to the H6573 from Hamamatsu contains a detailed presentation of the operating mode.

generally varies. At least the phase of an RF output can be adjusted digitally in about 1° steps. In the case depicted in Figure 1, the phase of the PMT modulation voltage is varied in the phase shifter/amplifier PA by means of the phase shifter.

[00024] ~~*Description of the Operating Mode and the Related Advantages of the Method Presented*~~ The operating mode and the related advantages of the method in accordance with the first embodiment will now be described.

[00025] Using the conventional LSM design, the light of the modulated/pulsed laser light source is focused on the lens plane by means of the scan mirrors and the LSM scan optics. The fluorescence is focused, as in the confocal Zeiss LSM510, in the direction of reflection on the detection pin hole using a beam splitter, focusing lens, etc. The raster-shaped movement of the laser focus over the lens plane and the synchronized detection - in the now modulated - PMT result in a confocal image of the lens plane. By using the homodyne technique, the PMT signal at the output of the LP filter LPF (image 1) is a DC signal, which varies only as a function of the laser spot position (pixel). Through repeated scanning operations during multiple different relative phases of the light modulator and detection modulation, it is possible to detect the fluorescence lifetime contrast or to measure the fluorescence lifetime. The significant advantage lies in the fact that the conventional data acquisition unit of the LRM can be used. The lifetime contrast is calculated from image to image.

[00026] ~~*Image Digitizing to Produce the Lifetime Contrast in a Confocal Microscope Image and/or to Display the Confocal Lifetime Distribution of Dyes.*~~ Image digitizing to produce the lifetime contrast in a confocal microscope image and/or to display the confocal lifetime distribution of dyes is carried out in accordance with the following steps.

[00027] • In a first step in the ~~realization~~ embodiment presented here, a first phase of the PMT detector PMT1 is adjusted digitally. The adjustment is done, as described above, with the electronic ~~PA~~ phase shifter/amplifier PA; and the resulting DC signal of the PMT (following the usual conversion from current to voltage and the usual conversion from analog to digital) is registered by means of the usual (LSM) analysis electronics in ~~synchronism~~ synchronization with the scanner XYS and stored in the PC by means of a storage medium.

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[00031] The Fourier expansion is expressed by

$$I(\varphi + \varphi_\tau) = a_0 + a_1 \cdot \sin(\varphi) + b_1 \cdot \cos(\varphi) \quad (7)$$

~~With~~ with the fluorescence intensity of a pixel I and the corresponding Fourier coefficients a_0 , a_1 , b_1 , where.

$$a_0 = \bar{I} = \frac{1}{N} \sum_{n=0}^{n-1} I\left(\varphi_\tau + n \frac{2\pi}{N}\right)$$

$$a_1 = \frac{2}{N} \sum_{n=0}^{n-1} \sin\left(\frac{2\pi n}{N}\right) I\left(\varphi_\tau + \frac{2\pi}{N}\right) \quad (8)$$

$$b_1 = \frac{2}{N} \sum_{n=0}^{n-1} \cos\left(\frac{2\pi n}{N}\right) I\left(\varphi_\tau + n \frac{2\pi}{N}\right)$$

[00032] At the same time a_0, a_1, b_0 are the Fourier coefficients (per pixel), $N \geq 2$ the number of the stored phase images (or pixel intensity) $I = I(\phi)$.

[00033] The modulation depth M_τ and the phase shift can be expressed by the lifetime ϕ_τ using the Fourier coefficients.

$$M_\tau = \frac{\sqrt{a_1^2 + b_1^2}}{a_0} = \frac{1}{\sqrt{1 + \omega^2 \tau^2}} \quad (9)$$

$$\varphi_\tau = -1 \cdot \frac{a_1}{b_1} = \omega \tau \quad (10)$$

[00034] The modulation depth M is calculated pixel by pixel. $M = M(i, j) = M_{ij}$, (i, j , pixel indices). Similarly the phase shift $\phi = \phi(i, j) = \phi_{ij}$.

[00035] The image of the modulation depth M_{ij} , which is calculated pixel by pixel in this manner, and the phase shift ϕ_{ij} , are displayed on the monitor.

[00036] Another type of display is the τ imaging, that is the lifetime $\tau(M)_{ij}$ or $\tau(\phi)_{ij}$, calculated for τ by means of resolution equations (9) or (10) [Clegg], as described by Schneider et al.

$$\tau(M) = \frac{1}{\omega} \cdot \sqrt{\frac{1}{M^2} - 1} \quad (11)$$

$$\tau(\varphi) = \frac{1}{\omega} \tan(\varphi) \quad (12)$$

[00037] M and ϕ are calculated with the equation (9) or (10); and the Fourier coefficients a_ϕ , a_ψ , b_ψ , determined with equation (8), are calculated.

[00038] To increase the accuracy in determining the phase, it is also possible to use the optimized algorithm, presented in a paper, "Phase Evaluation by Folding," by Küchel, 1989.

Realization 2: Second Embodiment:

[00039] Another ~~realization~~ embodiment of a confocal microscope with lifetime contrast or for the measurement of the lifetime distribution in a confocal split image can be achieved using pulse lasers. Suitable are, for example, pulse laser diodes or other, for example fs ~~[= femtosecond]~~ femtosecond (fs) laser systems (for example, a Ti:sapphire laser), for example with a downstream frequency conversion unit (for example, frequency doubling, tripling). When pulse lasers are used, there is no need to generate the RF driver frequency with synthesizers. Instead, an electronic diode signal of the pulse laser is provided (for example, PD signal out of the fs/ps NIR laser in Figure 1 or an equivalent construction with exchange/expansion of the VIS laser module, for example with a ps diode laser etc.). The resulting RF signal of the (~~adequately~~ sufficiently fast) photodiode is a priori synchronized with the laser excitation. The RF signal can be used analogously with the RF signal of a synthesizer. That is, the phase shifter/amplifier PA ~~unit~~ is made available at the

corresponding input (by way of an RF line). The rest of the process is analogous to ~~realization 1~~ that of the first embodiment. What is advantageous here is, on the one hand, the use of a pulse-shaped light source and the associated improvement of the signal-to-noise ratio in a lifetime contrast, generated thereby, as compared to the sinusoidal modulation of the laser excitation in ~~realization 1~~ the first embodiment and, on the other hand, the omission of a synthesizer for generating the RF frequency. The fluorescence is detected after a 1 photon excitation (linear in the excitation intensity).

1.2 Two Photon Confocal Lifetime Imaging, Homodyne

[00040] ~~The object of this chapter is~~ A third embodiment, using the combination of 2-photon microscopy with the homodyne detection technique for lifetime imaging, will now be described.

[00041] The combination of time resolution and 2-photon microscopy was already demonstrated by Gratton with the so called heterodyne technique ~~[So]~~, as described by So et al., "Time Resolved Fluorescence Microscopy using Two Photon Excitation," *Bioimaging* 3 (1995) 49 (hereinafter, "So et al."). In the heterodyne technique an fs laser is used for fluorescence excitation in a 2-photon microscope; and the PMT detector is driven at a slightly different modulation frequency. The typical repetition rate of fs Ti:sapphire lasers is in the 80 MHz range. In ~~[So]~~ the So et al. article, a frequency of 80 MHz + 25 kHz is used for amplification modulation of the PMT detector. The consequence is a beat. This beat is digitized with an ADC ~~[= analog to digital conversion]~~ analog to digital conversion (ADC) card and scanned. Thus, it is possible to detect pixel by pixel the phase shift from excitation to fluorescence (heterodyne method).

[00042] In the design ~~presented here~~ in accordance with the present invention, the phase shift is determined, compared to ~~[So]~~ that described by So et al., not pixel by pixel, but rather image by image. That is, first one image is captured during a relative phase shift ϕ_1 and stored. In at least one other step, an image is generated during another different relative phase ϕ_2 (homodyne method).

[00043] The diverse images for presenting the contrast are calculated in the same manner as ~~in Chapter 1.1~~ described above in connection with the one-photon homodyne detection technique for confocal lifetime imaging.

[00044] **Procedure** The procedure by which 2-photon microscopy is combined with the homodyne detection technique for lifetime imaging will now be described.

[00045] A dyed or self-fluorescing sample is excited so as to emit fluorescence by way of two photon absorption. The pulsed laser can be, for example, a Ti:sapphire laser (also sums with double or triple frequency or a difference with mixed frequency, etc.), a ps laser diode or a laser, which is modulated, for example, by means of an AOM ~~[= acousto-optical modulator]~~ or EOM ~~[= electro-optical modulator]~~ optical modulator M, such as an acousto-optical modulator (AOM) or an electro-optical modulator (EOM). In ~~1.1~~ the first and second embodiments, the physical process is a one photon excitation; in ~~1.2~~ the third embodiment, it is two photon excitation (or in general multiphoton excitation). To excite the fluorescence in the realization embodiment according to Figure 1, an fs Ti:sapphire laser is used. The repetition rate of the fs laser is approximately 80 MHZ ~~(NLO-LSM~~ [=non-linear optics laser scanning microscope], non-linear optics laser scanning microscope (NLO-LSM), fluorescence detection method).

[00046] For detection, a modulatable PMT detector from Hamamatsu (H6573) is used. The sinusoidal modulation frequency is generated from a photodiode signal of the laser (fs Mira,

Coherent Corporation) by way of an ECL [~~emitter coupled logic~~] emitter coupled logic (ECL) logic circuit and amplified to an average power of 15.W at 50W by means of an RF amplifier, integrated into the ~~PA~~ phase shifter/amplifier PA, and is available at the output “RF out” of the PA. The phase of the generated sine (and thus the amplified sine) can be adjusted to approximately 1° (analogous to ~~Chapter 1.1~~ the first and second embodiments). The electronic jitter is < 100 ps ((Figure 1), phase shifter/RF amplifier). With the amplified sine wave at the frequency, corresponding to the laser repetition rate ($f_{rep} = f_{mod}$), the amplification of the PMT detector is modulated. To this end, the amplified RF frequency is made available to the input of the PMT module, called “RF modulation in” in Figure 1. The current at the output of the PMT detector is smoothed with a passive LP filter or is integrated by a different method by way of the integration circuit. The resulting DC signal is made available again to the detection unit of an LRM. The rest of the procedure for gathering and evaluating the data is analogous to that described in ~~Chapter 1.1~~ connection with the first and second embodiments.

[00047] The distinction with respect to ~~1.1~~ the first and second embodiments lies in the fact that in one case a two photon (NLO) LSM is combined with the lifetime imaging. That is, the fluorescence excitation occurs with an fs or ps pulse laser. Thus, another significant difference is the type of fluorescence excitation (here two or generally multiphotons (> 2) excitation).

1.3 Arrangement for Phase Sensitive Fluorescence Detection in a Laser Scanning Microscope

[00048] For two or multiphoton excitation, it is possible to use more efficient detection units due to the depth discriminated excitation. They are described in the literature under the collective term of non-descanned detection units.

[00049] This detection unit is shown in Figure 2 as a schematic drawing, which is attached to the scan lens SL and the scanner XYS of Figure 1 and depicts a microscope beam path, with the sample P, the lens OL, the beam splitter ST for coupling in the illumination/coupling out the radiation, coming from the sample, as well as a first tube lens TL1.

[00050] By way of a second tube lens TL2 TQ, another modulatable PMT, designated PMT2 in Figure 2, is used for direct detection in a detection beam path DE, that is, not by way of a scan beam path.

[00051] This PMT is connected to the control unit ST CU in Figure 1 and by way of said control unit CU to other units in Figure 1.

[00052] A significant drawback with these detection units is generally their higher sensitivity to room light. Since the room light is generally not modulated, or differently is modulated differently from excitation light, the use of phase sensitive detection units for suppressing the room light is logical. Thus, there is no need for an expensive encapsulation of the detection unit. The configurations for ~~1 and 2~~ one and two or multiphoton excitation have already been described above and are totally transferable to a phase sensitive detector. However, in the phase sensitive detection technique the reference signal (excitation light) and the measurement signal (fluorescence signal) have the same modulation. For most of the TiSa laser systems that are used, this modulation is 80 MHZ. Thus, homodyne detection takes place. For phase sensitive detection, both signals are multiplied together in a multiplier with a fixed variable phase relation. In an advantageous arrangement the first dynode of a modulatable photomultiplier (H6573) functions as the multiplier.

[00053] The reference signal is generated from the above described phase shifter/RF amplifier PA. The clock for the phase shifter is the photodiode signal of the pulse laser. In addition, the

repetition rate, predetermined by means of the pulse laser, can be expanded to a variable beat frequency range by "beating" the laser light with an optical modulator (AOM or EOM, M) (see Figure 1). The beat frequency is provided by means of a synthesizer with variable phase, which is controlled by means of trigger signals of the excitation light source (see Figure 1). The phase relation between the reference signal and the measurement signal is adjusted in such a manner that the phase shift is zero. Thus, the variable is demodulated. In this manner a DC or low frequency modulated measurement signal is obtained. However, disturbances, like room light, are highly modulated after the multiplier (like the reference signal approx. 80 MHz). Due to the downstream low pass filter the highly modulated portions (disturbances) are filtered out and thus suppressed. An example of the low pass filter is the detection electronics of a conventional LSM.

[00054] The advantage of the described arrangement lies in the fact that the electronics on the detection side has to be designed only for low frequency signals, since the demodulation takes place in the photomultiplier.

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IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

In re Application of:

Volker GERSTNER et al.

U.S. Application No. 09/869,317

Internat'l Appl. No. PCT/EP00/11626

Internat'l Appl. Filed: November 22, 2000

For: METHOD FOR DETECTING
FLUORESCENCE PHENOMENA
IN MICROSCOPE

Art Unit: (not yet assigned)

Examiner: (not yet assigned)

Atty Docket: P66886US0

REQUEST FOR APPROVAL OF PROPOSED DRAWING CORRECTIONSCommissioner for Patents
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Sir:

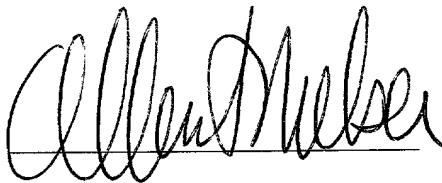
Please amend the drawings as indicated in red in the accompanying photocopies, and advise
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Respectfully submitted,

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WO 01/38856

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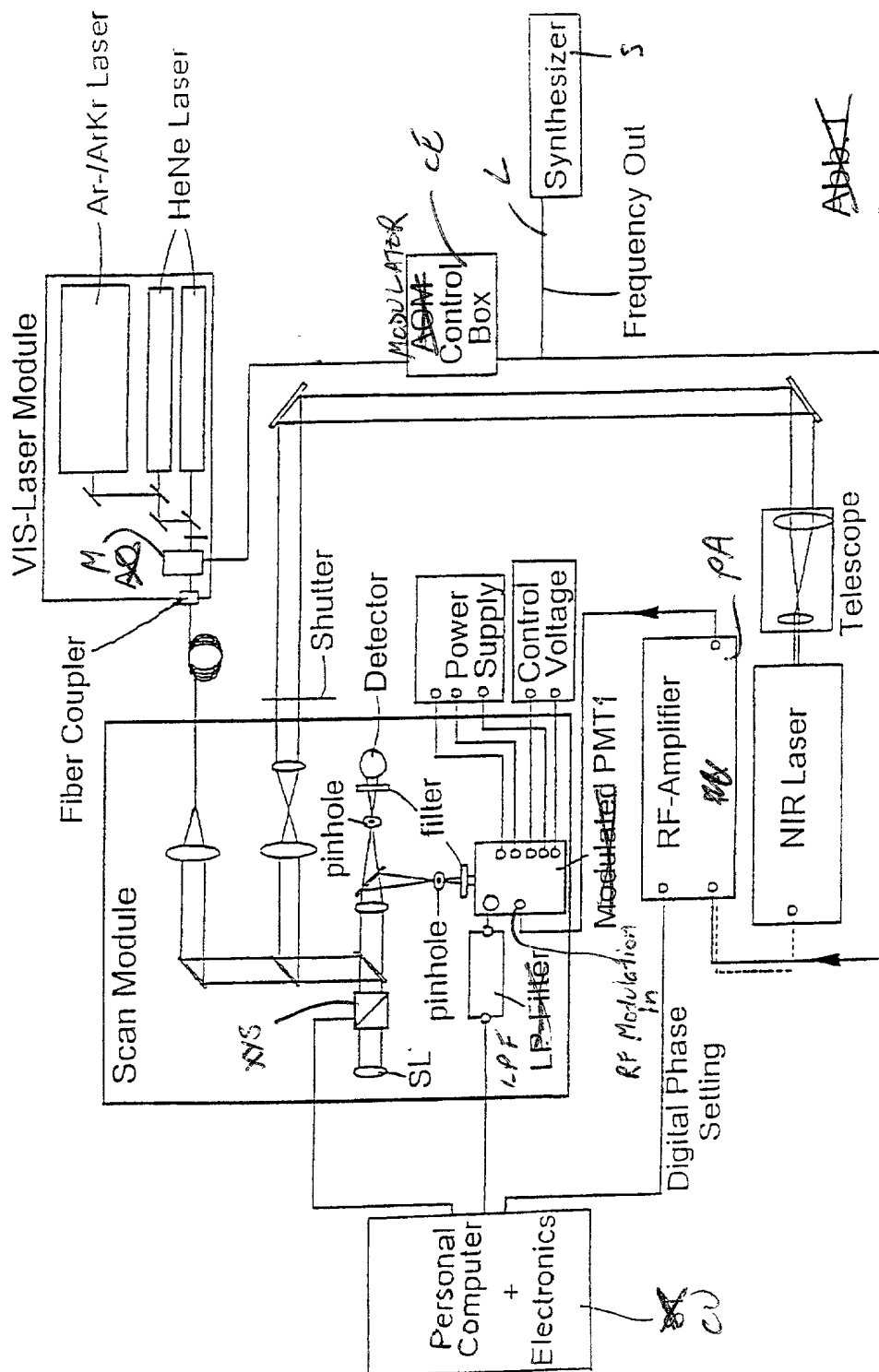
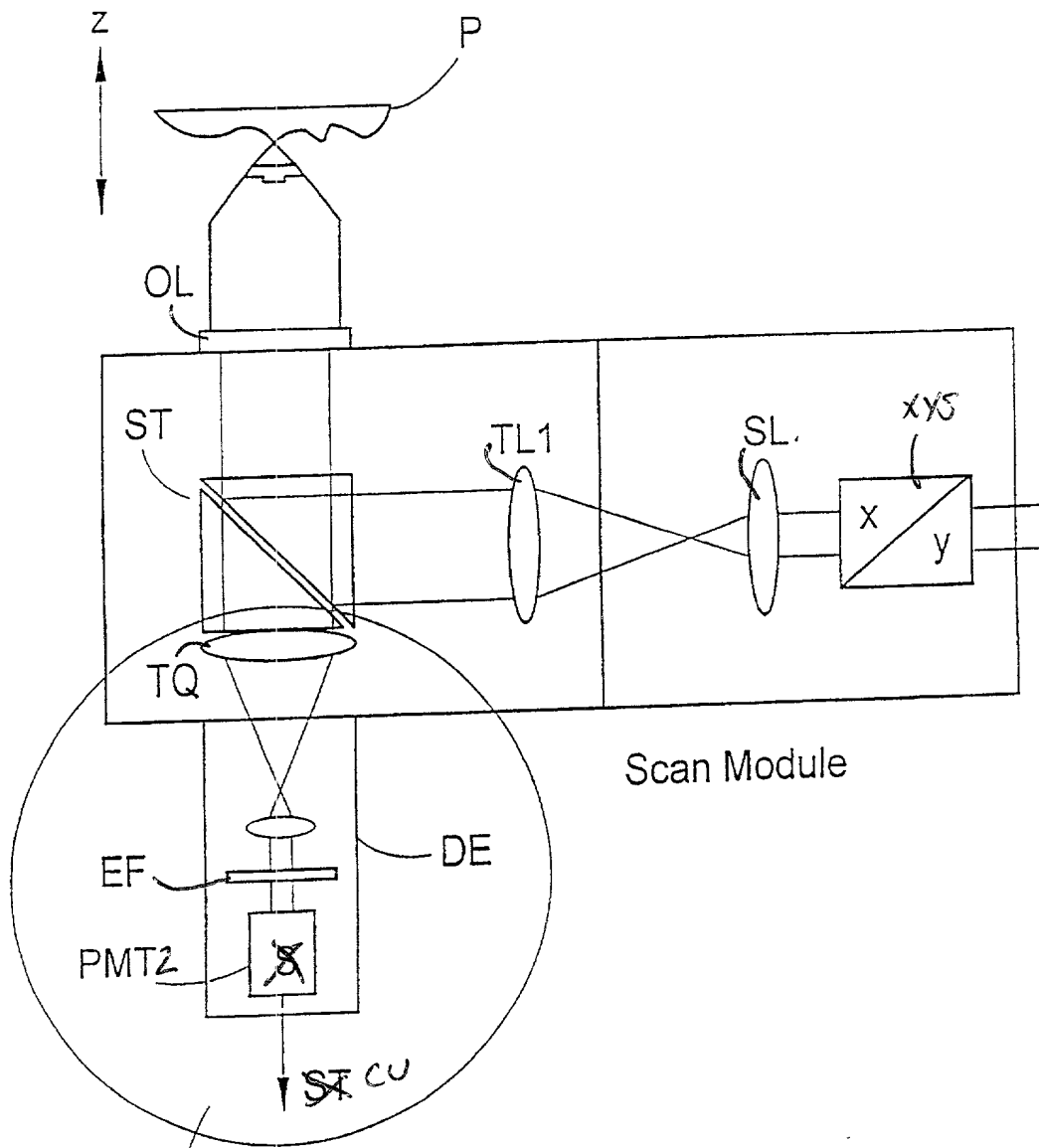


Abb. 1
Fig. 1



Scan Module

nicht descant
Non-descanned

Abb. 2 Fig. 2

2/2

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TRANSLATION CERTIFICATION

This is to certify that the translation of the attached documents: **Basic German Application No: PCT/EP00/11626; Case Reference No.: 12732/P66886US0;** and document **WO 01 / 38856 Literature** is to the best of our knowledge and ability, a true and accurate translation of the original text delivered to us by our client **JACOBSON HOLMAN**. The original document was to be translated from **German into English**, and said translation was completed and delivered to the client on October 26, 2001.

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District of Columbia) ss:

BE IT KNOWN, that on the 26th day of October 2001 before me a Notary Public in and for the District of Columbia, duly commissioned and sworn, personally came and appeared Mr. Ernest Oropeza who acknowledged that he executed the within instrument

IN TESTIMONY WHEREOF, I have hereunto subscribed my name and affixed my seal of office, the day and year above written

Tanja L. Baybrook
MS. TANJA L. BAYBROOK
NOTARY PUBLIC, DISTRICT OF COLOMBIA
MY COMMISSION EXPIRES ON DECEMBER 14, 2005

09869317-24 DEC 2001

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Process for the Detection of the Phenomenon of Fluorescence
in a Microscope

The process that is presented relates to confocal and 2 photon fluorescence microscopy [Goeppert] [Wilson]. Both methods are assumed to be known.

Both confocal fluorescence microscopy and 2 photon microscopy are modified by the method presented below to the extent that an additional contrast parameter is possible: the fluorescence lifetime.

Temporal resolved fluorescence and / or the use of the lifetime as a contrast parameter in confocal / 2 photon microscopy can be carried out by two different methods - by time domain detection and frequency domain detection.

In the case of **time domain detection** [Wabnitz] [Gröbler] a fluorescent sample is excited so as to produce fluorescence by means of a pulsed light source, and the fluorescence emission is detected with time resolution either by means of time correlated single photon counting (TCSPC) [Müller] [Han] or by means of time gated detection [Schbg] [Cubeddu] [Dowling].

In the case of **frequency domain detection**, a fluorescent sample or preparation is excited with a light source that is either actively modulated or pulsed (for example, by means of passive mode coupling). Since any arbitrary modulation of the excitation by means of a Fourier analysis falls part into sinusoidal components, the observation of a sinusoidal excitation is adequate. The frequency domain detection technique is based on the delay of the fluorescence emission by a phase ϕ and a change in the modulation depth M compared with the excitation light as a function of the modulation frequency ω ($=2\pi f_{\text{mod}}$) and the lifetime τ .

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$$\varphi = \text{atan}(\omega \tau) \quad (1)$$

$$M = 1 / \sqrt{1 + \omega^2 \tau^2} \quad (2)$$

However, the resulting fluorescence signal, oscillated with the modulation frequency, is out of phase and demodulated. For typical fluorescence lifetimes ranging from $\tau = 1 \dots 10$ ns, modulation frequencies ranging from $f_{\text{mod}} = 10 \dots 100$ MHz are adequate.

Since it generally does not make any sense to scan the fluorescence signal at such high modulation frequencies, a frequency mixing process is used to detect the signal. For mixing, any detection element with a modulatable amplification is suitable.

In essence two methods are distinguished - the homodyne and the heterodyne detection techniques.

To understand the principle, one observes generally two "signals" S_1, S_2 , (for example S_1 modulated excitation, S_2 modulated amplification).

$$\begin{aligned} S_1 &= A_0 + A_1 \cos(\omega_a t + \alpha) \\ S_2 &= B_0 + B_1 \cos(\omega_b t + \beta) \end{aligned} \quad (3)$$

Multiplication results in:

$$\begin{aligned} S_1 S_2 &= A_0 B_0 + A_0 B_1 \cos(\omega_b t + \beta) + B_0 A_1 \cos(\omega_a t + \alpha) + \\ &\quad A_1 B_1 \{ \cos((\omega_a + \omega_b)t + (\alpha + \beta)) + \cos((\omega_a - \omega_b)t + (\alpha - \beta)) \} \end{aligned} \quad (4)$$

Homodyne Detection

If $\omega_a = \omega_b$ (homodyne), the second harmonic and a frequency independent component are generated by the mixing process of the "signals" S_1 and S_2 . A low pass filter results in a suppression of the components at ω_a and $2\omega_a$. Only the

The DC background and the phase dependent DC component are detected. The signal, filtered by means of a low pass (LP = low pass), can be written as:

$$LP(S_1 S_2) = A_0 B_0 + A_1 B_1 \cos(\alpha - \beta) \quad (5)$$

In the case of homodyne detection this frequency independent (DC) signal can be detected in multiple relative phases. To measure the fluorescence lifetime, at least 3 different phase positions are necessary. At just two relative phase positions, the phase shift or the demodulation, induced by the fluorescence lifetime, can be used as the contrast parameter (Clegg).

Heterodyne Detection - Cross Correlation

If $\omega_b = \omega_a + \Delta\omega$ (heterodyne), the mixing process generates a high frequency signal at the total frequency and a signal at the cross correlation frequency $\Delta\omega$. Again the high frequency components are suppressed by a low pass filter.

$$LP(S_1 S_2) = A_0 B_0 + A_1 B_1 \cos(\Delta\omega t + \alpha - \beta) \quad (6)$$

In the case of heterodyne detection, the differential frequency $\Delta\omega$ is detected. Phase position and modulation depth of the signal at the differential frequency make it possible to determine the lifetime. Typical cross correlation frequencies range from a few Hz up to about 100 kHz.

A more comprehensive presentation of the heterodyne method can be found in the publication by E. Gratton et al. [Gratton] [Gratton 2].

In both the homodyne and heterodyne detection technique the high frequency change is reflected, so to say, on the low frequency range.

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Owing to the multi-exponential decay behavior of the fluorescence emission, the lifetimes, determined from the modulation depth and the phase shift, vary. Therefore, for precise measurement of the lifetime, the excitation frequency has to be varied [Gratton2].

If, in contrast, the lifetime is supposed to be used, for example, as a contrast parameter in an imaging process, this is generally not necessary. Frequently it suffices, for example, to show the phase shift or the demodulation by means of the lifetime or by means of the lifetime, calculated from the phase shift and demodulation data, at a fixed modulation frequency.

1.1 Confocal Lifetime Imaging, Homodyne

The confocal design of an LSM [= laser scanning microscope] is modified for lifetime imaging to the extent that

- the excitation light source is modulated or a pulse laser is used.
- the amplification of the detector (for example, PMT) is modified.
- an electronic phase shifter is used that permits the relative phase position of light excitation and detection to be adjusted. This circuit with the components that are used is shown in Figure 1.

Realization 1:

Driven by means of a synthesizer S using a quartz crystal, RF frequencies are generated in the range from 10 to 100 MHz. The output of the synthesizer S is connected, on the one hand, over a shielded high frequency line (for example, over a BNC cable) to a phase shifter / amplifier PA. The phase shifter / amplifier amplifies, on the one hand, the high frequency input signal of the synthesizer - in the presented realization to a power of approx. 1.5 W at a resistance of 50W. Furthermore, the phase position of the amplified RF signal can be varied with the PA. The relative phase of the PA can be adjusted digitally over a control line, for example, by means of a control via a serial interface of a PC. The amplified RF signal is fed to a

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modulated PMT [= photomultiplier tube] - for example, the PMT module (H 6573) from Hamamatsu.¹ The amplified RF voltage (approximately 25 V_{pp} / 50W) is fed in the PMT to the second dynode and used to modulate the amplification of the PMT. To produce a defined low pass filter, the output signal of the PMT can be smoothed by means of a commercial low pass (LP) filter. The 3 dB threshold frequency f_g of the LP filter is selected in such a manner that

$$1 / \text{pixel dwell time} \ll f_g \ll f_{\text{laser}}$$

where f_{laser} = the laser modulation frequency. The signal filtered thus is fed to the standard detection electronics of the LRM [= laser raster microscope]. (For greater comprehension: in principle, for example, to an ADC (analog digital converter), which is synchronized with the xy scanners of the LRM.

A second identical output of the synthesizer S is also connected to the control electronics of the light modulator M by means of a high frequency line. An acousto-optical modulator (or an electro-optical modulator) can be used, for example, as the modulator in the laser beam path. The light modulator is a component of the laser module of the confocal laser raster microscope. Such a design makes it possible to vary the relative phase position of the PA and the light modulator M. The frequencies for M for modulating the laser light and the PMT amplification voltage are identical. The phase position generally varies. At least the phase of an RF output can be adjusted digitally in about 10 steps. In the case depicted in Figure 1, the phase of the PMT modulation voltage is varied in PA by means of the phase shifter.

Description of the Operating Mode and the Related Advantages of the Method Presented

Using the conventional LSM design, the light of the modulated / pulsed laser light source is focussed on the lens plane by means of the scan mirrors and the LSM scan optics. The fluorescence is focussed, as in the confocal Zeiss LSM510,

¹ The "Technical Information" to the H6573 from Hamamatsu contains a detailed presentation of the operating mode.

in the direction of reflection on the detection pin hole using a beam splitter, focussing lens, etc. The raster-shaped movement of the laser focus over the lens plane and the synchronized detection - in the now modulated - PMT result in a confocal image of the lens plane. By using the homodyne technique, the PMT signal at the output of the LP filter (image 1) is a DC signal, which varies only as a function of the laser spot position (pixel). Through repeated scanning operations during multiple different relative phases of the light modulator and detection modulation, it is possible to detect the fluorescence lifetime contrast or to measure the fluorescence lifetime. The significant advantage lies in the fact that the conventional data acquisition unit of the LRM can be used. The lifetime contrast is calculated from image to image.

Image Digitizing to Produce the Lifetime Contrast in a Confocal Microscope Image and / or to Display the Confocal Lifetime Distribution of Dyes.

- In a first step in the realization presented here, a first phase of the PMT detector is adjusted digitally. The adjustment is done, as described above, with the electronic PA phase shifter / amplifier; and the resulting DC signal of the PMT (following the usual conversion from current to voltage and the usual conversion from analog to digital) is registered by means of the usual (LSM) analysis electronics in synchronism with the scanner and stored in the PC by means of a storage medium.
- In at least a second step the process is repeated with a second different relative phase position.

The at least two digital images are displayed, for example, by means of a computer screen without any further calculation.

For the presentation, images, generated with the following algorithms, are also displayed on the screen (Fourier expansion):

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The Fourier expansion is expressed by

$$I(\varphi + \varphi_\tau) = a_0 + a_1 \bullet \sin(\varphi) + b_1 \bullet \cos(\varphi) \quad (7)$$

With the fluorescence intensity of a pixel I and the corresponding Fourier coefficients a_0, a_1, b_1 .

$$\begin{aligned} a_0 = \bar{I} &= - \frac{1}{N} \sum_{M=0}^{M-1} I(\varphi_\tau + n \frac{2\pi}{N}) \\ a_1 &= - \frac{2}{N} \sum_{n=0}^{n-1} \sin(\frac{2\pi n}{N}) I(\varphi_\tau + n \frac{2\pi}{N}) \\ b_1 &= - \frac{2}{N} \sum_{M=0}^{M-1} \cos(\frac{2\pi n}{N}) I(\varphi_\tau + n \frac{2\pi}{N}) \end{aligned} \quad (8)$$

At the same time a_0, a_1, b_0 are the Fourier coefficients (per pixel); $N \geq 2$ the number of the stored phase images (or pixel intensity) $\neq (\varphi)$.

The modulation depth M_τ and the phase shift can be expressed by the lifetime φ_τ using the Fourier coefficients.

$$M_\tau = \frac{\sqrt{(a_1^2 + b_1^2)}}{a_0} = \frac{1}{\sqrt{(1 + \omega^2 \tau^2)}} \quad (9)$$

$$\varphi_\tau = -1 \bullet \frac{a_1}{b_1} = \omega \tau \quad (10)$$

The modulation depth M is calculated pixel by pixel. $M = M(i,j) = M_U, (i,j, \text{pixel indices})$. Similarly the phase shift $\varphi = \varphi(i,j) = \varphi_U$.

The image of the modulation depth M_U , which is calculated pixel by pixel in this manner, and the phase shift φ_U , are displayed on the monitor.

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Another type of display is the τ imaging, that is the lifetime $\tau(M)_{i,j}$ or $\tau(\phi)_{i,j}$, calculated for τ by means of resolution equations (9) or (10) [Clegg].

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$$\tau(M) = 1/\omega \bullet \sqrt{[(1 / (M^2) - 1]} \quad (11)$$

$$\tau(\omega) = \frac{1}{\omega} \tan(\varphi) \quad (12)$$

M and φ are calculated with the equation (9) or (10); and the Fourier coefficients a_0 , a_1 , b_1 , determined with equation (8), are calculated.

To increase the accuracy in determining the phase, it is also possible to use the optimized algorithm, presented in a paper, Phase Evaluation by Folding, by Küchel, 1989.

Realization 2:

Another realization of a confocal microscope with lifetime contrast or for the measurement of the lifetime distribution in a confocal split image can be achieved using pulse lasers. Suitable are, for example, pulse laser diodes or other, for example fs [= femtosecond] laser systems (Ti:sapphire laser), for example with downstream frequency conversion unit (for example, frequency doubling, tripling). When pulse lasers are used, there is no need to generate the RF driver frequency with synthesizers. Instead, an electronic diode signal of the pulse laser is provided (for example, PD signal out of the fs / ps NIR laser in Figure 1 or an equivalent construction with exchange / expansion of the VIS laser module, for example with a ps diode laser etc.). The resulting RF signal of the (adequately fast) photodiode is a priori synchronized with the laser excitation. The RF signal can be used analogously with the RF signal of a synthesizer. That is, the phase shifter / amplifier PA unit is made available at the corresponding input (by way of an RF line). The rest of the process is analogous to realization 1. What is advantageous here is, on the one hand, the use of a pulse-shaped light source and the associated improvement of the signal-to-noise ratio in a lifetime contrast, generated thereby, as compared to the sinusoidal modulation of the laser excitation in realization 1 and, on the other hand, the omission of a synthesizer for generating the RF frequency. The fluorescence is detected after a 1 photon excitation (linear in the excitation intensity).

1.2 Two Photon Confocal Lifetime Imaging, Homodyne

The object of this chapter is the combination of 2 photon microscopy with the homodyne detection technique for lifetime imaging.

The combination of time resolution and 2 photon microscopy was already demonstrated by Gratton with the so-called heterodyne technique [So]. In the heterodyne technique an fs laser is used for fluorescence excitation in a 2 photon microscope; and the PMT detector is driven at a slightly different modulation frequency. The typical repetition rate of fs Ti:sapphire lasers is in the 80 MHz range. In [So] a frequency of 80 MHz + 25 kHz is used for amplification modulation of the PMT detector. The consequence is a beat. This beat is digitized with an ADC [= analog to digital conversion] card and scanned. Thus, it is possible to detect pixel by pixel the phase shift from excitation to fluorescence (heterodyne method).

In the design presented here, the phase shift is determined, compared to [So], not pixel by pixel, but rather image by image. That is, first one image is captured during a relative phase shift ϕ_1 and stored. In at least one other step, an image is generated during another different relative phase ϕ_2 (homodyne method).

The diverse images for presenting the contrast are calculated in the same manner as in Chapter 1.1.

Procedure

A dyed or self-fluorescing sample is excited so as to emit fluorescence by way of two photon absorption. The pulsed laser can be, for example, a Ti:sapphire laser (also sums with double or triple frequency or a difference with mixed frequency, etc.), a ps laser diode or a laser, which is modulated, for example, by means of an AOM [= acousto-optical modulator] or EOM [= electro-optical modulator]. In 1.1. the physical process is a one photon excitation; in 1.2 it is two photon excitation (or in general multiphoton excitation). To excite the fluorescence in the realization according to Figure 1, an fs Ti:sapphire laser is used. The repetition rate of the fs laser is approximately 80 MHz (NLO - LSM [= non-linear optics laser scanning microscope], fluorescence detection method).

For detection, a modulatable PMT detector from Hamamatsu (H6573) is used. The sinusoidal modulation frequency is generated from a photodiode signal of the laser (fs Mira, Coherent Corporation) by way of an ECL [= emitter coupled logic] logic circuit and amplified to an average power of 15. W at 50W by means of an RF amplifier, integrated into the PA phase shifter / amplifier, and is available at the output "RF out" of the PA. The phase of the generated sine (and thus the amplified sine) can be adjusted to approximately 1° (analogous to Chapter 1.1). The electronic jitter is < 100 ps ((Figure 1), phase shifter / RF amplifier). With the amplified sine wave at the frequency, corresponding to the laser repetition rate ($f_{rep} = f_{mod}$), the amplification of the PMT detector is modulated. To this end, the amplified RF frequency is made available to the input of the PMT module, called "RF modulation in" in Figure 1. The current at the output of the PMT detector is smoothed with a passive LP filter or is integrated by a different method by way of the integration circuit. The resulting DC signal is made available again to the detection unit of an LRM. The rest of the procedure for gathering and evaluating the data is analogous to that described in Chapter 1.1.

The distinction with respect to 1.1. lies in the fact that in one case a two photon (NLO) LSM is combined with the lifetime imaging. That is, the fluorescence excitation occurs with an fs or ps pulse laser. Thus, another significant difference is the type of fluorescence excitation (here two or generally multiphotons (> 2) excitation).

1.3 Arrangement for Phase Sensitive Fluorescence Detection in a Laser Scanning Microscope

For two or multiphoton excitation, it is possible to use more efficient detection units due to the depth discriminated excitation. They are described in the literature under the collective term of non-descanned detection.

This detection is shown in Figure 2 as a schematic drawing, which is attached to the scan lens SL and the scanner of Figure 1 and depicts a microscope beam path, with the sample P, the lens OL, the beam splitter ST for coupling in the

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the illumination / coupling out the radiation, coming from the sample, as well as a first tube lens TL1.

By way of a second tube lens TL2, another modulatable PMT is used for direct detection in a detection beam path DE, that is, not by way of a scan beam path.

This PMT is connected to the control unit ST in Figure 1 and by way of said control unit to other units in Figure 1.

A significant drawback with these detection units is generally their higher sensitivity to room light. Since the room light is generally not or differently modulated from excitation light, the use of phase sensitive detection units for suppressing the room light is logical. Thus, there is no need for an expensive encapsulation of the detection unit. The configurations for 1 and 2 or multiphoton excitation have already been described above and are totally transferable to a phase sensitive detector. However, in the phase sensitive detection technique the reference signal (excitation light) and the measurement signal (fluorescence signal) have the same modulation. For most of the TiSa laser systems that are used, this modulation is 80 MHz. Thus, homodyne detection takes place. For phase sensitive detection, both signals are multiplied together in a multiplier with a fixed variable phase relation. In an advantageous arrangement the first dynode of a modulatable photomultiplier (H6573) functions as the multiplier.

The reference signal is generated from the above described phase shifter / RF amplifier. The clock for the phase shifter is the photodiode signal of the pulse laser. In addition, the repetition rate, predetermined by means of the pulse laser, can be expanded to a variable beat frequency range by "beating" the laser light with an optical modulator (AOM or EOM, see Figure 1). The beat frequency is provided by means of a synthesizer with variable phase, which is controlled by means of trigger signals of the excitation light source (see Figure 1). The phase relation between the reference signal and the measurement signal is adjusted in such a manner that the phase shift is zero. Thus, the variable is demodulated. In this manner a DC or low frequency modulated measurement signal is obtained. However, disturbances, like room light, are highly modulated

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after the multiplier (like the reference signal approx. 80 MHz). Due to the downstream low pass filter the highly modulated portions (disturbances) are filtered out and thus suppressed. An example of the low pass filter is the detection electronics of a conventional LSM.

The advantage of the described arrangement lies in the fact that the electronics on the detection side has to be designed only for low frequency signals, since the demodulation takes place in the photomultiplier.

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Patent Claims

1.

Process for detecting the phenomenon of fluorescence in a microscope, wherein the sample is irradiated by a modulated and / or pulsed laser light source, and the fluorescence is detected at least in two different phase positions of the detector.

2.

Process, as claimed in claim 1, wherein an image is produced for each phase position.

3.

Process, as claimed in at least one of the preceding claims, wherein the generated images or the images, calculated from these images, are displayed on a monitor.

4.

Process, as claimed in at least one of the preceding claims, wherein the illumination and the detection take place by way of a laser scanning microscope.

5.

Process, as claimed in at least one of the preceding claims, wherein the detection takes places with a modulatable PMT.

6.

Process for detecting the phenomenon of fluorescence in a microscope, wherein the sample is irradiated by a modulated and / or pulsed laser light source, wherein a reference signal, corresponding to the modulated and / or pulsed laser, and a measurement signal, corresponding to a modulated detection, are multiplied together with a fixed variable phase relation; and the result serves to display the image.

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7.

Process, as claimed in claim 6, wherein the phase relation is adjusted in such a manner that the phase shift is zero.

8.

Process, as claimed in any of the claims 6 or 7, with non-descanned detection.

9.

Application of a process, according to any one of the preceding claims, to the multiphoton excitation of fluorescence emission, in particular two photon excitation.

10.

Process, as claimed in any one of the preceding claims, with the use of a cw laser, modulated by means of an acousto-optical modulator (AOM).

11.

Process, as claimed in any one of the preceding claims, with the use of a cw laser, modulated by means of a Pockel cell.

12.

Process, as claimed in any one of the preceding claims, with the use of a pulse laser, which is additionally modulated.

13.

Process, as claimed in any one of the preceding claims, with the use of a pulse laser, which is additionally modulated by means of an AOM.

14.

Process, as claimed in any one of the preceding claims, with the use of a pulse laser, which is additionally modulated by means of a Pockel cell.

15.

Process, as claimed in any one of the preceding claims, for use for time resolution of multiphoton processes, like second harmonic generation on surfaces or two photon excitation.

16.

Process, as claimed in any one of the preceding claims, with the use of a pulsed near infrared (NIR) laser.

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17.

Process, as claimed in any one of the preceding claims, with the use of a pulsed near infrared (NIR) laser with downstream frequency conversion to 1 photon excitation.

18.

Process, as claimed in any one of the preceding claims, with the use of a pulsed near infrared (NIR) laser with downstream frequency conversion to 1 photon excitation of fluorescence.

19.

Process, as claimed in any one of the preceding claims, with the use of phase sensitive detection for improving the signal to noise ratio.

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Key to figures:

Abb. 1 = Figure 1

Abb. 2 = Figure 2

nicht descannt = non-descanned

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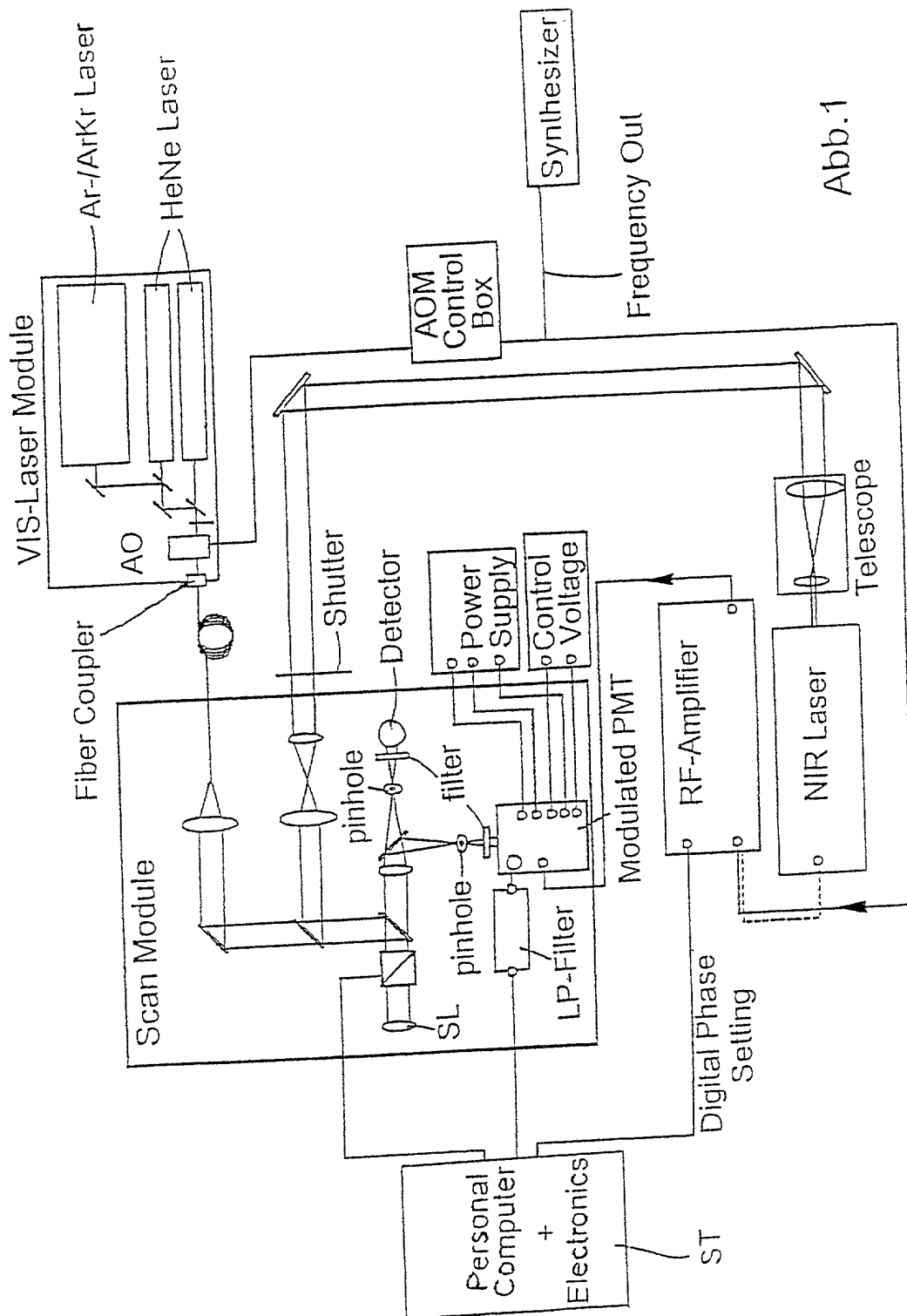


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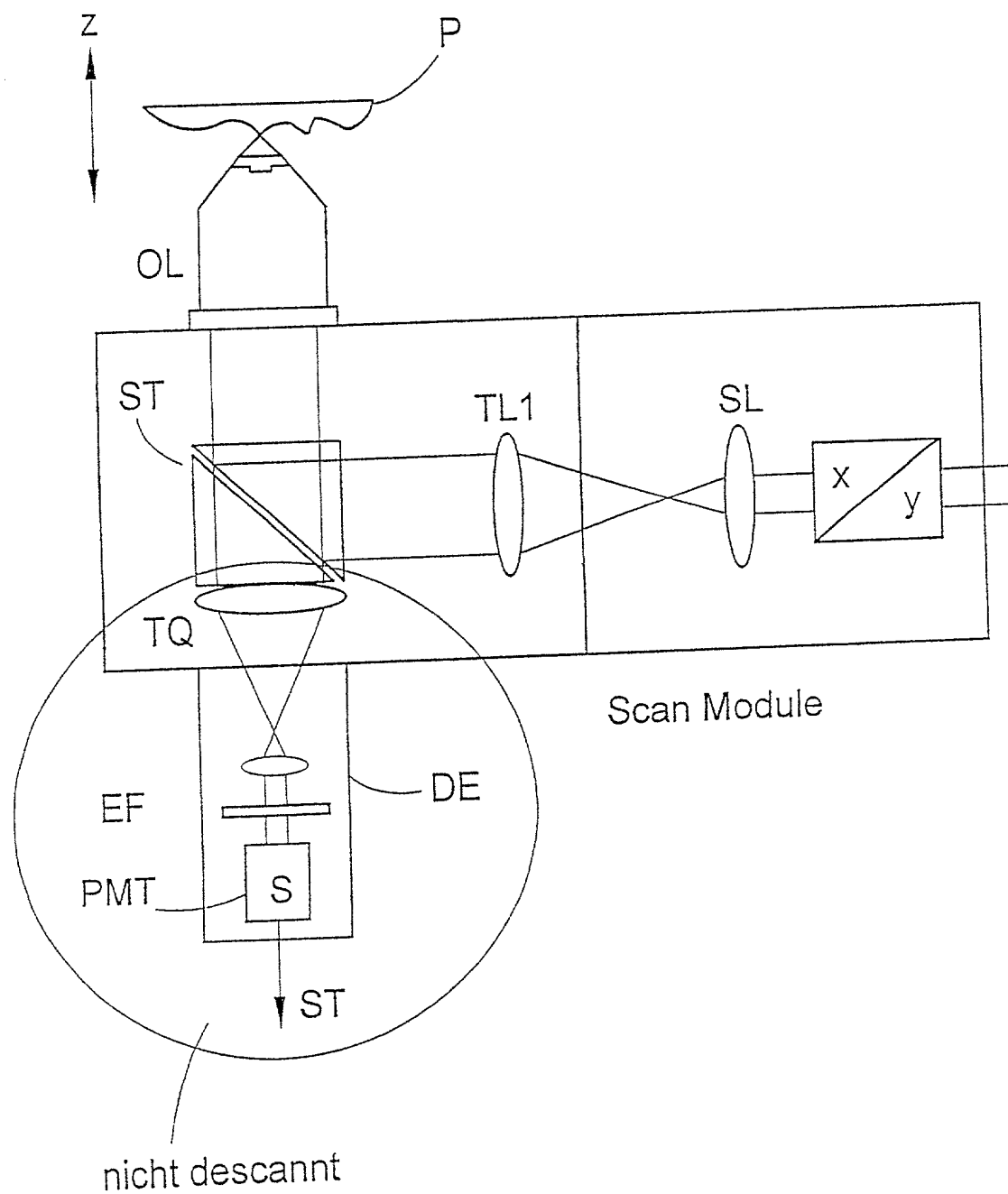


Abb. 2

DECLARATION
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U.S.A.

ALL PATENTS, INCLUDING DESIGN
FOR APPLICATION BASED ON PCT; PARIS CONVENTION;
NON PRIORITY; OR PROVISIONAL APPLICATIONS

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P66886US0

As a below named inventor, I declare that my residence, post office address and citizenship are stated below next to my name, the information given herein is true, that I believe that I am the original, first and sole inventor (if only one name is listed at 201 below), or an original, first and joint inventor (if plural inventors are named below at 201-203, or on additional sheets attached hereto) of the subject matter which is claimed and for which patent is sought on the invention entitled:

METHOD FOR DETECTING FLUORESCENCE PHENOMENA IN MICROSCOPE

which is described and claimed in:

☒ PCT International Application No. PCT/EP00/11626

filed November 22, 2000

☐ the attached specification

☒ the specification in application Serial No. 09/869,317

filed July 24, 2001

(if applicable) and amended on _____

I hereby state that I have reviewed and understand the contents of the above-identified specification, including the claims, as amended by any amendment referred to above. I acknowledge the duty to disclose information which is material to patentability as defined in Title 37, Code of Federal Regulations, §1.56.

I hereby claim foreign priority benefits under Title 35, United States Code, §119 (a)-(d) of any foreign application(s) for patent or inventor's certificate listed below and have also identified below any foreign application for patent or inventor's certificate having a filing date before that of the application on which priority is claimed.

Prior Foreign Application(s)

199 56 620.8
(Number)

GERMANY
(Country)

25 November 1999
(Day/Month/Year Filed)

Priority Claimed

☒
Yes

☐
No

(Number)

(Country)

(Day/Month/Year Filed)

☐
Yes

☐
No

(Number)

(Country)

(Day/Month/Year Filed)

☐
Yes

☐
No

I hereby claim the benefit under Title 35, United States Code, §119(e) of any United States provisional application(s) listed below:

Application No. _____ Filing Date _____ Application No. _____ Filing Date _____

I hereby claim the benefit under Title 35, United States Code, §120 of any United States application(s) listed below and, insofar as the subject matter of each of the claims of this application is not disclosed in the prior United States application in the manner provided by the first paragraph of Title 35, United States Code, §112, I acknowledge the duty to disclose information which is material to patentability as defined in Title 37, Code of Federal Regulations, §1.56 which became available between the filing date of the prior application and the national or PCT international filing date of this application:

(Application Serial No.)

(Filing Date)

(Status: patented, pending, abandoned)

POWER OF ATTORNEY: As a named inventor, I hereby appoint the following attorneys (Registration No.) to prosecute this application, receive and act on instructions from my agent, and transact all business in the Patent and Trademark Office connected therewith HARVEY B. JACOBSON, JR. (20,851), JOHN CLARKE HOLMAN (22,769), MARVIN R. STERN (20,640), ALLEN S. MELSER (27,215), MICHAEL R. SLOBASKY (26,421), JONATHAN L. SCHERER (29,851), IRWIN M. AISENBERG (19,007), WILLIAM E. PLAYER (31,409); YUON S. HAM (45,307) and NATHANIEL A. HUMPHRIES (22,772)

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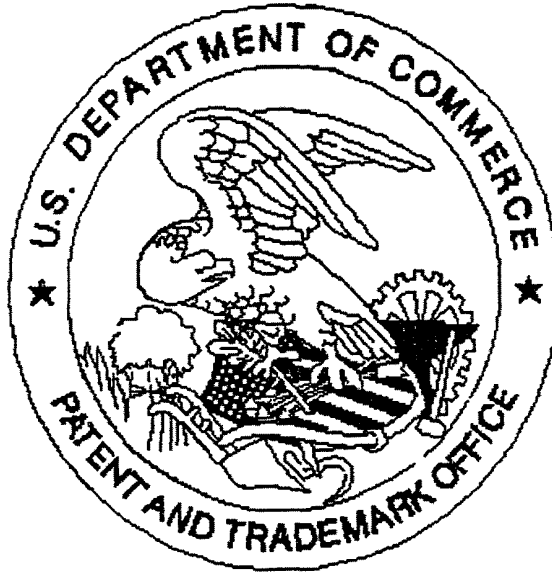
SIGNATURE OF INVENTOR 201*	SIGNATURE OF INVENTOR 202*	SIGNATURE OF INVENTOR 203*
<u>[Signature]</u>	<u>[Signature]</u>	
DATE <u>8.10.01</u>	DATE <u>8.10.2001</u>	DATE

☐ Additional inventors are named on separately numbered sheets attached hereto

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